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# Inference for a Simple Step-Stress Model for the Extension of Exponential Distribution under Progressive Type-II Censored Competing Risks Data

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## 1. Introduction

In reliability analysis, it's common to consider several causes, either mechanical or electrical, those competing to fail a unit. These causes are called "competing risks." The main problem of reliability studying or life testing experiments is that units' failure connects with more than one cause of failure. In practice, the failure causes may be independent or dependent.

Although a dependent risk structure might be more realistic, there is a concern about the identifiability of the underlying model. Without the information on covariates, it's not possible to test the assumption of s-independent risks, as discussed by Crowder (1991) and Kalbfleisch and Prentice (2011). Thus, in most



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cases, for analyzing a competing risks model, the causes of failure are assumed to be independent. A series system with multiple components can also be treated as an independent competing risks model. By assuming independence among competing failure causes, many authors have investigated the competing risks models, such as David and Moesch Berger (1978), Sarhan et al. (2010), and Crowder (2001). Censoring is common in life tests for saving time and cost reduction. There are different types of censoring schemes. The most popular censoring schemes are Type-I and Type-II censoring schemes. In the Type-I censoring scheme, the test is terminated at fixed  $T \in (0, \infty)$  and uses the observed samples until T. In the Type-II censoring scheme, the test is terminated when samples are observed until the predetermined observation number (r). Different types of mixtures of these two basic censoring schemes are known as hybrid censoring schemes. It was first introduced by Epstein (1954), in the state of life-testing Experiments.

The hybrid censoring schemes have been studied under different lifetime distributions, by several authors. Compared to the conventional Type-I and Type-II censoring schemes, progressive censoring provides higher flexibility to the experimenter by allowing the tested units to be removed at non-terminal time points. This allowance may be desirable when some degradation-related information from live test specimens needs to be collected and analyzed, or when scarce testing facilities need to be released for other experiments. So progressive Type-II censoring is highly efficient and effective in utilizing the available resources. Although censoring can help shorten the time and reduce the cost, with more and more products possessing high quality and long life, censoring can't meet the demands of collecting enough information about the products' lifetimes as soon as possible. One way to overcome this problem is accelerated life tests (ALTs) [see Nelson (1990)]. So, the ALTs are widely used in reliability analysis. Shi et al. (2013) considered a constant stress accelerated life test (CSALT) with competing risks for failure from exponential distribution under progressive Type II hybrid censoring. The maximum likelihood estimator and Bayes estimator of the parameter were derived. Xu and Tang (2011) and Wu et al. (2014) considered different inferential issues regarding the constant-stress accelerated competing failure models when the lifetime of different risk factors follows Weibull distributions. Based on Nelson's cumulative exposure (CE) model.

Balakrishnan and Han (2008) and Han and Balakrishnan (2010) developed the exact inference for a simple step-stress model with competing risks for failure from the exponential distribution under Type-II and Type-I censoring schemes, respectively. Liu and Shi (2017) considered a simple step-stress model with progressively censored competing risk data from the Weibull distribution. El-Shahat et al. (2025) considered a simple step-stress model with Type-I censored competing risks data from Rayleigh distribution. Also, Han and Kundu (2014) introduced a step-stress model with competing risks for failure from the generalized exponential distribution under Type-I censoring. Recently, the progressive Type-II censoring scheme has become quite popular for analyzing highly reliable data.

# 2. Progressive Type-II Censoring Scheme

Progressive Type-II censoring was introduced by Cohen (1963). This type of censoring scheme can be described as: Suppose *n* identical items are put to test; the integer  $m \le n$  is a pre-specified number of failures and  $R_1, R_2, ..., R_m$  are *m* prefixed integers satisfying  $R_1 + R_2 + \cdots + R_m + m = n$ . At the time of the first failure  $t_{1:m:n}, R_1$  of the surviving units are randomly withdrawn. Likewise, at the time of the second failure  $t_{2:m:n}, R_2$  of the surviving units are randomly withdrawn, and so on. At the time of the *ith* failure  $t_{i:m:n}$ , the experiment stopped and all surviving  $R_i = n - m - (R_1 + \cdots + R_{(m-1)})$  units are withdrawn. For more details about progressive Type-II censoring, the experiment is stopped, and all



surviving [Equation]units are withdrawn. For more details about progressive Type-II censoring, Balakrishnan and Aggarwala. (2000), and Balakrishnan and Cramer. (2014).



Figure 1. Progressive Type-II Censoring Scheme

Nadarajah and Haghighi (2011) introduced an extension of the exponential distribution as an alternative to gamma, Weibull, and generalized exponential distributions. It has an increasing as well as a decreasing failure rate depending on the values of the shape parameter. It has an increasing (decreasing) failure rate function when ( $\alpha > 1$ ), ( $\alpha < 1$ ), it respectively, and for  $\alpha = 1$  becomes constant. The extension of the exponential distribution specified by the probability density function (PDF):

$$f(t) = \alpha \beta (1 + \beta t)^{\alpha - 1} e^{[1 - (1 + \beta t)^{\alpha}]} , t > 0, \alpha, \beta > 0.$$
  
The corresponding cumulative distribution function (CDF) is

$$F(t) = 1 - e^{[1 - (1 + \beta t)^{\alpha}]}, t > 0, \alpha, \beta > 0$$
(1)

and the corresponding hazard rate function (HRF) is given by:

$$h(t) = \alpha \beta (1 \beta t)^{\alpha - 1}$$
<sup>(2)</sup>

where  $\beta$  is the scale parameter, and  $\alpha$  is the shape parameter.

This research is organized as follows; Section 3 introduces the model formulation. The classical maximum likelihood estimation (MLEs) and the asymptotic confidence intervals (CIs) of the unknown parameters are discussed in Section 4. In Section 5, The Bayes estimates (BEs) of model parameters using the Markov chain Monte Carlo (MCMC) method are obtained. In Section 6, the performance of these confidence/credible intervals is evaluated in terms of probability coverages via Monte Carlo simulations. In Section 7, we present a numerical example to illustrate all the methods of inference developed in this article, and some concluding remarks are finally made in Section 8.

## 3. Model description and test assumptions

Let  $s_0$  denote the normal stress level. Consider *n* identical units being placed on a simple step-stress ALT under the initial stress level  $s_1(s_1 > s_0)$  See Chapter 2 of Nelson (1990) for further information on accelerated models.

The successive failure times are recorded along with the information about which risk factor causes each failure. At a pre-fixed time  $\tau \in (0, \infty)$ , the stress level is increased from  $s_1 to s_2$  and the life test continues until the *mth* (*m* is pre-fixed) failure is observed. At the  $(1 \le i \le m - 1)$  failure time,  $R_i$  of the surviving items are randomly removed, where  $R_i$  is pre-fixed and  $R_m = n - m - \sum_{i=1}^{m-1} R_i$ .



#### **Basic Assumptions**

- 1. The failure of a product occurs only due to one of the two independent competing failures caused by lifetimes.  $T_1$  and  $T_2$ . Then, the failure time of the product  $T = min(T_1, T_2)$ .
- 2. Two stress levels  $s_1$  and  $s_2(s_1 < s_2)$  are used (simple step stress).
- 3. For any stress level  $s_i$ , the lifetime of the *jth* failure cause  $T_{ij}$ , (i, j = 1, 2) follows an extension of the exponential distribution with a scale parameter  $\beta_{ij}$  and shape parameter  $\alpha_{ij}$ .
- 4. The failure mechanisms are the same under different stress levels, i.e.  $\alpha_{1j} = \alpha_{2j} = \alpha_j$
- 5. The accelerated function (AF) of the *jth* failure cause is log-linear, namely.

$$ln(\beta_{ij}) = a_j + b_j \,\varphi(s_i) \,, i, j = 1, 2 \quad, \tag{3}$$

where  $a_j$ ,  $b_j$  are unknown parameters,  $\varphi(s_i)$  is a given decreasing function of stress level *s*. We adopt the Arrhenius model in this article, so  $\varphi(s_i) = 1/s_i$ .

6. The cumulative exposure model holds, see (Nelson, 1990). From the assumption of the cumulative exposure model and the CDF given in Eq. (1), the CDF of the lifetime  $T_{ij}$  under the simple step-stress ALT are given as

$$G_{j}(t) = \begin{cases} F_{1}(t) = 1 - e^{\left[1 - (1 + \beta_{1j}t)^{\alpha_{j}}\right]} & \text{if } 0 < t < \tau \\ F_{2}(t - \tau + u) = 1 - e^{\left[1 - (1 + \beta_{2j}(t - \tau) + \beta_{1j}\tau)^{\alpha_{j}}\right]} & \text{if } \tau \le t < \infty \end{cases}$$
(4)

Where the equivalent starting time u is the solution of  $F_2(u) = F_1(\tau)$  for j=1, 2. The corresponding probability density function (PDF) of  $T_j$  is given by

$$g_{j}(t) = \begin{cases} f_{1}(t) = \alpha_{j} \beta_{1j} \left(1 + \beta_{1j}\right)^{\alpha_{j}-1} e^{\left[1 - \left(1 + \beta_{1j}t\right)^{\alpha_{j}}\right]} & \text{if } 0 < t < \tau \\ f_{2}(t - \tau + u) = \alpha_{j} \beta_{2j} \left(1 + \beta_{2j}(t - \tau) + \beta_{1j}\tau\right)^{\alpha_{j}} e^{\left[1 - \left(1 + \beta_{2j}(t - \tau) + \beta_{1j}\tau\right)^{\alpha_{j}-1}\right]} & \text{if } \tau \leq t < \infty \end{cases}$$

$$\tag{5}$$

for j = 1, 2.

Since we will observe only the smaller of  $T_1$  and  $T_2$ , let  $T = \min(T_1, T_2)$  note the overall failure time of a test unit. Then, its CDF and PDF are readily obtained to be

$$F_{T}(t) = 1 - (1 - G_{1}(t))(1 - G_{2}(t))$$

$$F_{T}(t) = \begin{cases} 1 - \{e^{[1 - (1 + \beta_{11}t)^{\alpha_{1}}]}\}\{e^{[1 - (1 + \beta_{12}t)^{\alpha_{2}}]}\} & \text{if } 0 < t < \tau \\ 1 - \{e^{[1 - (1 + \beta_{21}(t - \tau) + \beta_{11}\tau)^{\alpha_{1}}]}\}\{e^{[1 - (1 + \beta_{22}(t - \tau) + \beta_{12}\tau)^{\alpha_{2}}]}\} & \text{if } \tau \le t < \infty \end{cases}$$
(6)

$$\begin{split} f_{T}(t) &= \\ \begin{cases} \alpha_{1}\beta_{11}(1+\beta_{11}t)^{\alpha_{1}-1}+\alpha_{2}\beta_{12}(1+\beta_{12}t)^{\alpha_{2}-1} \ e^{[1-(1+\beta_{11}t)^{\alpha_{1}}]+[1-(1+\beta_{12}t)^{\alpha_{2}}]} & \text{if } 0 < t < \tau \\ \alpha_{1}\beta_{21}(1+\beta_{21}(t-\tau)+\beta_{11}\tau)^{\alpha_{1}-1}+\alpha_{2}\beta_{22}(1+\beta_{22}(t-\tau)+\beta_{12}\tau)^{\alpha_{2}-1} \\ &\times \ e^{[1-(1+\beta_{21}(t-\tau)+\beta_{11}\tau)^{\alpha_{1}}]+[1-(1+\beta_{22}(t-\tau)+\beta_{12}\tau)^{\alpha_{2}}]} & \text{if } \tau \leq t < \infty \end{split}$$

$$\end{split}$$

$$(7)$$

Let  $\delta$  be the indicator of the failure cause, then we derive the joint PDF of  $(T, \delta)$  as

$$f_{T,\delta}(t,j) = g_j(t) \left( 1 - G_{j}(t) \right)$$



$$\begin{split} f_{T,\delta}(t,j) &= \\ \begin{cases} \alpha_{j}\beta_{1j} \big(1+\beta_{1j}t\big)^{\alpha_{j}-1} \ e^{[1-(1+\beta_{11}t)^{\alpha_{1}}]+[1-(1+\beta_{12}t)^{\alpha_{2}}]} & \text{if } 0 < t < \tau \\ \alpha_{j}\beta_{2j} \big(1+\beta_{2j}(t-\tau)+\beta_{1j}\tau\big)^{\alpha_{j}-1} e^{[1-(1+\beta_{21}(t-\tau)+\beta_{11}\tau)^{\alpha_{1}}]+[1-(1+\beta_{22}(t-\tau)+\beta_{12}\tau)^{\alpha_{2}}]} & \text{if } \tau \leq t < \infty \end{split}$$

$$\end{split}$$

$$\end{split}$$

$$\end{split}$$

for  $j, j^{`} = 1, 2$  and  $j \neq j^{`}$ .

Suppose there are  $N_1$  failures before the stress changing time  $\tau$ . If we denote  $n_{1j}$  and  $n_{2j}$  (j = 1,2) as the number of failures due to failure causes j under stress level  $s_1$  and  $s_2$ , respectively, then  $N_1 = n_{11} + n_{12}$ and  $m - N_1 = n_{21} + n_{22}$  is the number of failures under stress level  $s_2$ . Since each failure time is accompanied by the corresponding cause of failure. Let  $\delta = (\delta_1, \delta_2, ..., \delta_m)$  be the observed sequence of the cause of failure corresponding to the observed failure time  $t = (t_1, t_2, ..., t_m)$ .

#### 4. Maximum Likelihood Estimates

Under the assumption of the cumulative exposure model, we formulate the likelihood function of  $\Theta$  =  $(\alpha_i, \beta_{1i}, \beta_{2i})$  based on the progressive Type-II censored data as

$$L \propto \prod_{i=1}^{N_1} f_{T,\delta}(t_i, \delta_i) \left[1 - F(t_i)\right] \prod_{i=N_1+1}^m f_{T,\delta}(t_i, \delta_i) \left[1 - F(t_i)\right]^{R_i}$$
(9)

$$L \propto \prod_{i,j=1}^{2} \alpha_{j}^{n_{ij}} \beta_{ij}^{n_{ij}} \prod_{i=1}^{N_{1}} (1 + \beta_{1j}t_{i})^{\alpha_{j}-1} e^{(R_{i}+1)\left[1 - (1 + \beta_{1j}t_{i})^{\alpha_{j}}\right]} \times \prod_{i=N_{1}+1}^{m} (1 + \omega(t_{i}))^{\alpha_{j}-1} e^{(R_{i}+1)\left[1 - (1 + \omega(t_{i}))^{\alpha_{j}}\right]}$$
re,  $\omega(t_{i}) = \{\beta_{2i}(t_{i} - \tau) + \beta_{1i}\tau\}$ 
(10)

wher e,  $\omega(t_i) = \{p_{2j}(t_i - \tau) + p_{1j}\tau\}$ 

Then the logarithm of likelihood function Eq. (10) of  $\alpha_{j}$ ,  $\beta_{1j}$  and  $\beta_{2j}$  is given by:

$$lnL \propto n_{ij}ln\alpha_{j} + n_{1j}ln\beta_{ij} + n_{2j}ln\beta_{2j} + (\alpha_{j} - 1)\sum_{i=1}^{N_{1}}ln(1 + \beta_{1j}t_{i}) + \sum_{i=1}^{N_{1}}(R_{i} + 1)[1 - (1 + \beta_{1j}t_{i})^{\alpha_{j}}] + (\alpha_{j} - 1)\sum_{i=N_{1}+1}^{m}ln(1 + \omega(t_{i})) + \sum_{i=N_{1}+1}^{m}(R_{i} + 1)[1 - (1 + \omega(t_{i}))^{\alpha_{j}}]$$
(11)

## **4.1 Point Estimation**

The MLEs of the parameters  $\alpha_j$ ,  $\beta_{1j}$  and  $\beta_{2j}$  can be obtained by setting the first partial derivative of Eq. (11) about  $\alpha_i$ ,  $\beta_{1i}$  and  $\beta_{2i}$  to zero, namely

$$\frac{\partial lnL}{\partial \alpha_j} = \frac{\sum_{i=1}^2 n_{ij}}{\alpha_j} + \sum_{i=1}^{N_1} ln(1+\beta_{1j}t_i) - \sum_{i=1}^{N_1} (R_i+1)(1+\beta_{1j}t_i)^{\alpha_j} ln(1+\beta_{1j}t_i) + \sum_{i=N_1+1}^m ln(1+\omega(t_i)) - \sum_{i=N_1+1}^{N_1} (R_i+1)(1+\omega(t_i))^{\alpha_j} ln(1+\omega(t_i))$$
(12)



$$\frac{\partial lnL}{\partial \beta_{1j}} = \frac{n_{1j}}{\beta_{1j}} + (\alpha_j - 1) \sum_{\substack{i=1\\m}}^{N_1} \frac{t_i}{(1 + \beta_{1j}t_i)} - \alpha_j \sum_{\substack{i=1\\m}}^{N_1} (R_i + 1) t_i (1 + \beta_{1j}t)^{\alpha_j - 1} + (\alpha_j - 1) \sum_{\substack{i=N_1+1\\m}}^{M_1} \frac{\tau}{(1 + \omega(t_i))} - \alpha_j \sum_{\substack{i=N_1+1\\m}}^{M_2} (R_i + 1) \tau (1 + \omega(t_i))^{(\alpha_j - 1)}$$
(13)

$$\frac{\partial lnL}{\partial \beta_{2j}} = \frac{n_{2j}}{\beta_{2j}} + \sum_{i=N_1+1}^{m} \frac{(t_i - \tau)}{(1 + \omega(t_i))} - \alpha_j \sum_{i=N_1+1}^{m} (R_i + 1) (t_i - \tau) (1 + \omega(t_i))^{(\alpha_j - 1)}$$
(14)

Now, we have a system of six nonlinear equations in six unknowns  $\alpha_j$ ,  $\beta_{1j}$  and  $\beta_{2j}$  a closed-form solution is quite difficult to obtain. Consequently, an iterative procedure such as the Newton-Raphson algorithm can be used to obtain a numerical solution of the above nonlinear system.

#### 4.2 Asymptotic Confidence Intervals

The asymptotic variance and covariance matrix of maximum likelihood estimates is given by the elements of the inverse of the Fisher information matrix as follows.

$$I_{ij}(\Theta) = E\{-\frac{\partial^2 lnL}{\partial \theta_i \,\partial \theta_j}\}$$

However, the exact mathematical expressions for the previous expectation are often difficult to obtain (Cohen, 1965). Therefore, the Fisher information matrix is approximated as

$$I_{ij}(\Theta) \approx \{-\frac{\partial^2 lnL}{\partial \theta_i \,\partial \theta_j}\}$$

The asymptotic variance-covariance matrix is defined by inverting the Fisher information matrix  $I_{ij}^{-1}(\Theta)$  as follows:

$$I^{-1}(\alpha_{j},\beta_{1j},\beta_{2j}) = \begin{bmatrix} L_{11} & L_{12} & L_{13} \\ L_{21} & L_{22} & L_{23} \\ L_{31} & L_{32} & L_{33} \end{bmatrix}_{\alpha_{j},\beta_{ij}=\widehat{\alpha_{j}},\widehat{\beta_{ij}}}^{-1}$$

here,

$$L_{11} = \frac{\partial^2 lnL}{\alpha_j^2} = -\frac{\sum_{i=1}^2 n_{ij}}{\alpha_j^2} - \sum_{i=1}^{n_1} (R_i + 1) (1 + \beta_{1j} t_i)^{\alpha_j} \left[ ln(1 + \beta_{1j} t_i) \right]^2 - \sum_{i=n_1+1}^m (R_i + 1) (1 + \omega(t_i))^{\alpha_j} ln(1 + \omega(t_i))^2,$$

$$L_{12} = L_{21} = \frac{\partial^2 lnL}{\partial \alpha_j \beta_{1j}} = \sum_{i=1}^{n_1} \frac{t_i}{(1+\beta_{1j}t_i)} - \sum_{i=1}^{n_1} (R_i+1) t_i (1+\beta_{1j}t_i)^{\alpha_j-1} [1+\alpha_j ln(1+\beta_{1j}t_i)] + \sum_{i=n_1+1}^{m} \frac{\tau}{(1+\omega(t_i))} - \sum_{i=n_1+1}^{m} \tau (R_i+1)(1+\omega(t_i))^{\alpha_j-1} [1+\alpha_j ln(1+\omega(t_i))],$$

$$L_{13} = L_{31} = \frac{\partial^2 log L}{\partial \alpha_j \beta_{2j}}$$



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$$=\sum_{i=n_{1}+1}^{m} \frac{(t_{i}-\tau)}{(1+\omega(t_{i}))} - \sum_{i=n_{1}+1}^{m} (t_{i}-\tau)(R_{i}+1)(1+\omega(t_{i}))^{\alpha_{j}-1}[1+\alpha_{j}ln(1+\omega(t_{i}))]$$

$$L_{22} = \frac{\partial^2 log L}{\beta_{1j}^2} = -\frac{n_{1j}}{\beta_{1j}^2} - (\alpha_j - 1) \sum_{i=1}^{n_1} \frac{t_i^2}{(1 + \beta_{1j} t_i)^2} - \alpha_j (\alpha_j - 1) \sum_{i=1}^{n_1} (R_i + 1) t_i^2 (1 + \beta_{1j} t_i)^{\alpha_j - 2} - (\alpha_j - 1) \sum_{i=n_1+1}^{m} \frac{\tau^2}{(1 + \omega(t_i))^2} - \alpha_j (\alpha_j - 1) \sum_{i=n_1+1}^{m} (R_i + 1) \tau^2 (1 + \omega(t_i))^{\alpha_j - 2},$$

$$L_{23} = L_{32} = \frac{\partial^2 log L}{\partial \beta_{1j} \beta_{2j}}$$
  
=  $-(\alpha_j - 1) \sum_{i=n_1+1}^m \frac{\tau(t_i - \tau)}{(1 + \omega(t_i))^2} - \alpha_j (\alpha_j - 1) \sum_{i=n_1+1}^m (R_i + 1) \tau(t_i - \tau) (1 + \omega(t_i))^{\alpha_j - 2},$   
$$L_{33} = \frac{\partial^2 log L}{\beta_{2j}^2} = -\frac{n_{2j}}{\beta_{2j}^2} - (\alpha_j - 1) \sum_{i=n_1+1}^m \frac{(t_i - \tau)^2}{(1 + \omega(t_i))^2} - \alpha_j (\alpha_j - 1) \sum_{i=n_1+1}^m (R_i + 1) (t_i - \tau)^2 (1 + \omega(t_i))^{\alpha_j - 2}$$
(15)

Substitute the MLEs  $\hat{\alpha}_j$ ,  $\hat{\beta}_{1j}$  and  $\hat{\beta}_{2j}$  for  $\alpha_j$ ,  $\beta_{1j}$  and  $\beta_{2j}$ , the observed Fisher information matrix  $I_{ij}(\Theta)$  can be obtained. Upon inverting this matrix and denoting  $\hat{V}_{ij} = \hat{I}_{ij}^{-1}$  we derive the two-sided)  $100(1 - \gamma)$  ACIs for  $\alpha_j$ ,  $\beta_{1j}$  and  $\beta_{2j}$  as

$$\widehat{\alpha}_{j} \pm z_{\gamma/2} \sqrt{\widehat{V}_{ij}(1,1)} , \, \widehat{\beta_{1j}} \pm z_{\gamma/2} \sqrt{\widehat{V}_{ij}(2,2)} , \, \widehat{\beta_{2j}} \pm z_{\gamma/2} \sqrt{\widehat{V}_{ij}(3,3)}$$

respectively, where  $j = 1,2andz_{\gamma/2}$  is the  $(1 - z_{\gamma/2})$  th quantile of a standard normal distribution.

#### 5. Bayes Estimation

In this section, we consider the Bayesian estimates of unknown parameters. Bayesian estimation approach has received a lot of attention for ana

lyzing failure time data. It makes use of one's prior knowledge about the parameters and also takes into consideration the data available.

## **5.1 Point Estimation**

The square error (SE) loss function and linear exponential (LINEX) loss function are considered to obtain BEs of the model parameters  $\alpha_i$ ,  $\beta_{1i}$  and  $\beta_{2i}$  under progressive Type-II censoring.



## Under Squared Error Loss Function (SE)

The Bayes estimates of the unknown parameters  $\theta = \alpha_j$ ,  $\beta_{1j}$  and  $\beta_{2j}$ , j = 1,2 under (SE) denoted by  $\tilde{\theta}_{(BSE)}$ ; can be calculated through the following equations as follows

$$\tilde{\theta}_{(BSE)} = E(\theta|\underline{x}) = \int_0^\infty \theta \pi^*(\theta|\underline{x}) d\theta$$

#### Under LINEX Loss Function

Under the assumption that the minimal loss occurs at  $\theta = (\alpha_j, \beta_{1j}\beta_{2j}), j = 1, 2$ , the LINEX loss function can be expressed as

$$L_{BL}(\Delta) \propto e^{c\Delta} - c\Delta - 1, c \neq 1$$
(16)

where  $\Delta = (\hat{\theta} - \theta)$  is an estimate of  $\theta$ .

The posterior expectation of the LINEX loss function Eq. (16) is

$$E\left(L_{BL}(\hat{\theta}-\theta)\right) \propto e^{c\hat{\theta}} E\left[e^{c\hat{\theta}}\right] - c\left(\hat{\theta}-E\left[\theta\right]\right) - 1$$
<sup>(17)</sup>

The Bayes estimator of  $\theta$ , denoted by  $\hat{\theta}$  under LINEX loss function, is the value of  $\hat{\theta}$  which minimizes Eq. (17) .it is

$$\tilde{\theta}_{BL} = -\frac{1}{c} \log \left\{ E\left[e^{c\hat{\theta}}\right] \right\}$$
(18)

For Bayesian estimation, we need prior distribution for the parameters  $\alpha_j$ ,  $\beta_{1j}$  and  $\beta_{2j}$ . Therefore, we suppose the prior distribution of  $\alpha_j$  is non-informative prior

$$\pi(\alpha_j)=\frac{1}{\alpha_j}, \ \alpha_j>0.$$

We Assume that the model parameters  $\beta_{1j}$  and  $\beta_{2j}$  are independent with priors as:

$$\pi(\beta_{1j}) \propto \beta_{1j}^{\sigma_{1j}-1} e^{\lambda_{1j}\beta_{1j}}$$
,  $\sigma_{1j}$ ,  $\lambda_{1j}$ .

and

$$\pi(eta_{2j}) \propto eta_{2j}^{\sigma_{2j}-1} e^{\lambda_{2j}eta_{2j}}$$
 ,  $\sigma_{2j}$  ,  $\lambda_{2j}$ 

Respectively, many authors used the gamma prior for the scale and the shape parameters instead of the exponential prior because the gamma prior is wealthy enough to cover the prior belief of the experimenter. See (Nassar and Eiss, 2005) for Weibull distribution and Singh et al. (2014) for the extension of the exponential distribution. Thus, the joint prior PDF of  $\alpha_i$ ,  $\beta_{1i}$  and  $\beta_{2i}$  is given by:

$$\pi(\alpha_j,\beta_{1j}\beta_{2j}) \propto \alpha_j^{-1}\beta_{1j}^{\sigma_{1j}-1}\beta_{2j}^{\sigma_{2j}-1}e^{-(\lambda_{1j}\beta_{1j}+\lambda_{2j}\beta_{2j})}, \alpha_j,\beta_{1j}\beta_{2j} > 0$$
(19)

The joint posterior density function of the parameters  $\alpha_j$ ,  $\beta_{1j}$  and  $\beta_{2j}$  can be written from Eq. (10) and Eq. (19)

$$\pi^{*}(\alpha_{j},\beta_{1j}\beta_{2j}) = \frac{1}{\nu} \{\alpha_{j}^{n_{ij}-1}\beta_{1j}^{n_{1j}+\sigma_{1j}-1}\beta_{2j}^{n_{2j}+\sigma_{2j}-1} e^{-(\lambda_{1j}\beta_{1j}+\lambda_{2j}\beta_{2j})} \times \prod_{i=1}^{N_{1}} (1+\beta_{1j}t_{i})^{\alpha_{j}-1} e^{(R_{i}+1)\left[1-(1+\beta_{1j}t_{i})^{\alpha_{j}}\right]} \times \prod_{i=N_{1}+1}^{m} (1+\omega(t_{i}))^{\alpha_{j}-1} e^{(R_{i}+1)(1+\omega(t_{i}))^{\alpha_{j}}}$$
(20)

where,



$$\nu = \int_{0}^{\infty} \int_{0}^{\infty} \alpha_{j}^{n_{ij}-1} \beta_{1j}^{n_{1j}+\sigma_{1j}-1} \beta_{2j}^{n_{2j}+\sigma_{2j}-1} e^{-(\lambda_{1j}\beta_{1j}+\lambda_{2j}\beta_{2j})} \prod_{i=1}^{N_{1}} (1+\beta_{1j}t_{i})^{\alpha_{j}-1} \\ \times e^{(R_{i}+1)\left[1-(1+\beta_{1j}t_{i})^{\alpha_{j}}\right]} \prod_{i=N_{1}+1}^{m} (1+\omega(t_{i}))^{\alpha_{j}-1} e^{(R_{i}+1)(1+\omega(t_{i}))^{\alpha_{j}}}$$

is normalizing constant.

It may be noted here that the posterior distribution of  $(\alpha_j, \beta_{1j}, \beta_{2j})$  takes a ratio form that involves an integration in the denominator and cannot be reduced to a closed form. Hence, the evaluation of the posterior expectation for obtaining the Bayes estimator of  $\alpha_j, \beta_{1j}$  and  $\beta_{2j}$  will be tedious. Among the various methods suggested to approximate the ratio of integrals of the above form. Therefore, the MCMC technique is used to approximate these integrals.

## 5.2 Bayesian estimation using the MCMC method

In this subsection, the MCMC method is considered to generate samples from the posterior distribution and then compute the BEs of  $\alpha_j$ ,  $\beta_{1j}$  and  $\beta_{2j}$  under simple step-stress ALT using progressive Type-II censoring in the presence of competing causes of risks. From the joint posterior density function in Eq. (20), the conditional posterior distributions of  $\alpha_j$ ,  $\beta_{1j}$  and  $\beta_{2j}$  are given respectively by:

$$\pi^{*}(\alpha_{j}|\beta_{1j}\beta_{2j}) \propto \alpha_{j}^{n_{ij}-1} \prod_{i=1}^{n_{1}} (1+\beta_{1j}t_{i})^{\alpha_{j}-1} e^{(R_{i}+1)\left[1-(1+\beta_{1j}t_{i})^{\alpha_{j}}\right]} \times \prod_{i=N_{1}+1}^{n_{1}} (1+\omega(t_{i}))^{\alpha_{j}-1} e^{(R_{i}+1)(1+\omega(t_{i}))^{\alpha_{j}}}$$

$$\pi^{*}(\beta_{1j}|\alpha_{j},\beta_{2j}) \propto \beta_{1j}^{n_{1j}+\sigma_{1j}-1} e^{-\lambda_{1j}\beta_{1j}} \prod_{i=1}^{n_{1}} (1+\beta_{1j}t_{i})^{\alpha_{j}-1} e^{(R_{i}+1)\left[1-(1+\beta_{1j}t_{i})^{\alpha_{j}}\right]} \times \prod_{i=N_{1}+1}^{m} (1+\omega(t_{i}))^{\alpha_{j}-1} e^{(R_{i}+1)(1+\omega(t_{i}))^{\alpha_{j}}}$$

$$\pi^{*}(\beta_{2j}|\alpha_{j},\beta_{1j}) \propto \beta_{2j}^{n_{2j}+\sigma_{2j}-1} e^{-\lambda_{2j}\beta_{2j}} \prod_{i=N_{1}+1}^{m} (1+\omega(t_{i}))^{\alpha_{j}-1} e^{(R_{i}+1)(1+\omega(t_{i}))^{\alpha_{j}}}$$

$$(23)$$

The conditional posterior distributions of  $\alpha_j$ ,  $\beta_{1j}$  and  $\beta_{2j}$  in Eq. (21), Eq. (22), and Eq. (23) cannot be reduced analytically to well-known distribution. The Metropolis-Hastings algorithm is used to generate random samples from these distributions, see (Upadhyay and Gupta, 2010). For more information concerning the application of M-H, readers may refer to Robert et al. (1999). The following algorithm is proposed to compute Bayes estimators of  $U = U(\alpha_j, \beta_{1j}, \beta_{2j})$  under SE and LINEX loss functions.

## Algorithm (1)

- 1. Start with  $\alpha_j^{(0)} = \hat{\alpha}_{jMLE}, \beta_{1j}^{(0)} = \hat{\beta}_{1jMLE}, \beta_{2j}^{(0)} = \hat{\beta}_{2jMLE}$
- 2. Set i = 1.
- 3. Generate  $\alpha_j^{(i)}, \beta_{1j}^{(i)}$  and  $\beta_{2j}^{(i)}$  from  $N(\Theta^{(i-1)}, S_{\Theta}^2)$ , where  $\Theta = (\alpha_j, \beta_{1j}, \beta_{2j})$  and  $S_{\Theta}^2$  is found from the Var-Cov matrix for vector  $\Theta$ .



- 4. Compute the acceptance ratio  $A = \frac{L(\theta^{(i)})\pi(\theta^{(i)})}{L(\theta^{(i-1)})\pi(\theta^{(i-1)})}$
- 5. Accept the proposed value  $\theta^i$  with probability min(A, 1), Let  $\theta^* \to \theta^{(i)}$  (accept),  $\theta^* \to \theta^{(i-1)}$  (reject).
- 6. Set i = i + 1.
- 7. Repeat steps (3)-(6) K times.
- 8. The approximate means of U and  $e^{-cU}$  are given respectively by

$$E(U) = \frac{1}{K - M} \sum_{i=M+1}^{K} U\left(\alpha_{j}^{(i)}, \beta_{1j}^{(i)}, \beta_{2j}^{(i)}\right), \qquad (24)$$

$$E(e^{-cU}) = \frac{1}{K - M} \sum_{i=M+1}^{K} exp\{-cU(\alpha_j^{(i)}, \beta_{1j}^{(i)}, \beta_{2j}^{(i)})\}.$$
 (25)

Where M is the burn-in period. Then, from Eq. (24) and Eq. (25), the Bayes estimators of U under balanced SE and balanced LINEX loss functions are given respectively by

$$\widehat{U}_{SE} = \Omega \widehat{U}_{ML} + (1 - \Omega) E(U)$$
(26)

$$\widehat{U}_{LINK} = -\frac{1}{C} In \left[ \Omega e^{-c \widehat{U}_{ML}} + (1 - \Omega) E(e^{-c U}) \right]$$
(27)

The balanced loss functions are more general, which include the MLE and both symmetric and asymmetric BEs as special cases.

## 5.3 Highest Posterior Density (HPD) Interval

A  $100(1 - \gamma)$ \% posterior interval for a random quantity  $\Theta$  is the interval that has the posterior probability  $(1 - \gamma)$ , that  $\Theta$  exists in the interval where,

$$P(L \le \Theta \le U) = \int_{U}^{L} \pi^{*}(\Theta|t) d\Theta = 1 - \gamma$$

The credible CIs of  $\alpha_i$ ,  $\beta_{1i}$  and  $\beta_{2i}$  are obtained by the following algorithm.

## Algorithm (2)

- 1. Do steps [(1)-(7)] in algorithm (1)
- 2. Sort the posterior sample  $\{\Theta^{(i)}, i = 1, 2, ..., N\}$  to obtain the ordered values as  $\Theta^{(1)} \le \Theta^{(2)} \le \cdots \le \Theta^{(N)}$
- 3. Determine the number of values to include in the interval  $z = [N(1 \gamma)]$
- 4. Find the smallest interval width by computing  $W_i = \Theta^{(i+z)} \Theta^{(i)}$  Then,  $100(1-\gamma)$ \% credible
- 5. CI of  $\Theta$  is given by

$$HPD = \{\Theta^{(i_{min})}, \Theta^{(i_{min}+z)}\}$$

# 6. Simulation Study

In this sub-section, to analyze the performance of estimation methods, including MLE and Bayesian estimation, a Monte Carlo simulation study is employed, under progressive Type-II under step-stress for NH distribution in the presence of competing causes of risks. Following the algorithm (Balakrishnan and Sandhu,1995), 1000 observations are generated from NH distribution based on the following assumptions:



- 1. Parameters are given by:
  - $\beta_{11} = 0.25, \qquad \beta_{12} = 0.20, \qquad \beta_{21} = 0.50, \beta_{22} = 0.45, \alpha_1 = 1.45, \alpha_2 = 1.50$
- 2. Sample sizes of n = 60, n = 80, and n = 100.
- 3. Number of failures of progressive censoring: m = 30,40,60,80.

Removed items  $R_i$  are assumed to be different sample size n and number of failures m as shown in Table (1)

n	m	Censoring Schemes								
n	т	<i>S</i> <sub>1</sub>	<i>S</i> <sub>2</sub>	<i>S</i> <sub>3</sub>	<i>S</i> <sub>4</sub>	<i>S</i> <sub>5</sub>				
60	30	$(30, 0^{*29})$	$(15, 0^{*28}, 15)$	$(0^{*14}, 15, 15, 0^{*14})$	$(1^{*30}, 0^{*0})$	$(0^{*29}, 30)$				
00	40	$(20, 0^{*39})$	$(10, 0^{*38}, 10)$	$(0^{*19}, 10, 10, 0^{*19})$	$(1^{*20}, 0^{*20})$	$(0^{*39}, 10)$				
00	40	$(40, 0^{*39})$	$(20, 0^{*38}, 20)$	$(0^{*19}, 20, 20, 0^{*19})$	$(1^{*40}, 0^{*0})$	$(0^{*39}, 40)$				
80	60	$(20, 0^{*59})$	$(10, 0^{*58}, 10)$	$(0^{*29}, 10, 10, 0^{*29})$	$(1^{*20}, 0^{*40})$	$(0^{*59}, 20)$				
100	60	$(40, 0^{*59})$	$(20, 0^{*58}, 20)$	$(0^{*29}, 20, 20, 0^{*29})$	$(1^{*40}, 0^{*20})$	$(0^{*59}, 40)$				
	80	$(20, 0^{*79})$	$(10, 0^{*78}, 10)$	$(0^{*39}, 10, 10, 0^{*39})$	$(1^{*20}, 0^{*60})$	$(0^{*79}, 20)$				
60 80 100	30 40 40 60 60 80	$\begin{array}{c} \mathbf{S_1} \\ (30, 0^{*29}) \\ (20, 0^{*39}) \\ (40, 0^{*39}) \\ (20, 0^{*59}) \\ (40, 0^{*59}) \\ (20, 0^{*79}) \end{array}$	$\begin{array}{c} \mathbf{S_2} \\ (15, 0^{*28}, 15) \\ (10, 0^{*38}, 10) \\ (20, 0^{*38}, 20) \\ (10, 0^{*58}, 10) \\ (20, 0^{*58}, 20) \\ (10, 0^{*78}, 10) \end{array}$	$\begin{array}{c} \textbf{S_3} \\ (0^{*14}, 15, 15, 0^{*14}) \\ (0^{*19}, 10, 10, 0^{*19}) \\ (0^{*19}, 20, 20, 0^{*19}) \\ (0^{*29}, 10, 10, 0^{*29}) \\ (0^{*29}, 20, 20, 0^{*29}) \\ (0^{*39}, 10, 10, 0^{*39}) \end{array}$	$\begin{array}{c} \mathbf{S_4} \\ (1^{*30}, 0^{*0}) \\ (1^{*20}, 0^{*20}) \\ (1^{*40}, 0^{*0}) \\ (1^{*20}, 0^{*40}) \\ (1^{*40}, 0^{*20}) \\ (1^{*20}, 0^{*60}) \end{array}$	$S_{5}$ (0* <sup>29</sup> , 30) (0* <sup>39</sup> , 10) (0* <sup>39</sup> , 40) (0* <sup>59</sup> , 20) (0* <sup>59</sup> , 40) (0* <sup>79</sup> , 20)				

Table 1. Numerous patterns for removing items from life tests at different stages

Here,  $(5^{*3}, 0)$ , for example, means that the censoring scheme employed is (5,5,5,0).

Consider the temperature-accelerated levels as  $S_1 = 285K$ ,  $andS_2 = 335K$  and the use temperature is  $S_0 = 210K$ . The lifetimes of the two failure causes follow NH distributions with shape parameters  $\alpha_1 = and\alpha_2 = 1.5$ , respectively. If the AFs are given for the failure cause 1 by  $ln(\beta_{i1}) = -2.8801 + 425.8185/s_i$  and for failure cause 2 by  $ln(\beta_{i2}) = -1.3965 + 200.4975/s_i$  then  $\beta_{11} = 0.25$ ,  $\beta_{12} = 0.20$ ,  $\beta_{21} = and\beta_{22} = 0.4$ .

The lifetime of the two failure causes follows an expansion of NH distribution with recognized shape parameter  $\alpha_1, \alpha_2$ , respectively. The amount of the parameter was selected to be  $\beta_{11}, \beta_{12}, \beta_{21}, \beta_{22}$ . To clarify a specific scenario underneath each cause of failure the increase of stress level in our case of the study with the NH model will be achieved by increasing the rate of the scale parameter  $\beta_c$ , which will be reflected in shrinking the main time to failure.

Before continuing, first, the progressively censored Type-II is created through competing risks data utilizing the NH cumulative exposure model (CEM) for constant m,  $(R_1, R_2, ..., R_{m,n})$ , as shown below:

Step 1: Based on the algorithm proposed by Balakrishnan and Sandhu (1995), generating two samples that are progressively censored  $W_1, W_2, ..., W_m$  and  $U_1, U_2, ..., U_m$  from Uniform distribution (0,1).

**Step 2:** Calculating  $t_{11h}$  and  $t_{12h}$  using

$$U_h = 1 - e^{[1 - (1 + \beta_{11} t_{11})^{\alpha_1}]}$$

and

$$W_h = 1 - e^{[1 - (1 + \beta_{12} t_{12})^{\alpha_2}]}$$

the minimum of  $(t_{11h}, t_{12h})$  is registered as  $t_h^*$ , while the corresponding minimum index comes out of this condition  $(t_{11h} < t_{12h}, set \xi_h^* = 1;$  else set  $\xi_h^* = 2)$  for  $1 \le h \le N_1$ . **Step 3:** Let's assume that various values of stress changing time  $\tau$  as follows:

$$\tau = \frac{mean(t_h^*) + median(t_h^*)}{2}$$



Step 4: Find  $N_1$  such that  $t_{N_1}^* < \tau < t_{N_1+1}^*$ . Hence, put  $t_h = t_h^*$  and  $\xi_h = \xi_h^*$  for  $1 \le h \le N_1$ . Step 5: Generating  $t_{21h}$  and  $t_{22h}$  utilizing

$$U_h = 1 - e^{[1 - (1 + \beta_{21}(t_{21} - \tau) + \beta_{11}\tau)^{\alpha_1}]}$$

and

$$W_h = 1 - e^{[1 - (1 + \beta_{22}(t_{22} - \tau) + \beta_{12}\tau)^{\alpha_2}]}$$

for  $N_1 + 1 \le h \le m$ . The minimum values of  $(t_{21h}, t_{22h})$  assigned as  $t_h^*$ .

**Step 6:** Setting the value of  $t_h = t_h^*$  and  $\xi_h = \xi_h^*$  for  $N_1 + 1 \le h \le m$ . Then  $t_1, t_2, ..., t_m$  are the required order observation and  $\xi = [\xi_1, \xi_2, ..., \xi_m]$  the vector of the indices.

MLEs and related 95% asymptotic confidence intervals (Asy-CI) are produced based on the generated data. On deriving MLEs, Be aware that the initial assumed values are regarded as true parameter values.

We compute Bayesian estimates using informative priors for the Bayesian estimation method using 2.5 as a value for all hyperparameters. Such values of informative priors are plugged in to evaluate the required estimates. Through implementing the MH algorithm, the MLEs are used as initial guess values, as well as the corresponding variance-covariance matrix  $S_{\theta}$  of  $\ln(\hat{\theta})$ , where  $\theta = (\beta_{11}, \beta_{12}, \beta_{21}, \beta_{22}, \alpha_1, \alpha_2)$ . In the end, 2000 burn-in samples were deleted from the total of 10,000 generated samples by the posterior density and produced Bayes estimates under two loss functions, namely: squared error loss (SEL) function LINEX at v = -0.5, 0.5 Also, HPD interval estimates have been computed according to the technique of Chen and Shao (1999).

All the average estimates for methods are reported in Table (3) to Table (8) for different combinations of sample size n and number of stages m. Further, the first column donates the average estimates (Avg.) and in the second column, related means square errors (MSEs). For confidence intervals, we have asymptotic confidence intervals for MLEs and HPD for Bayesian estimates based on MCMC which are reported in Table (10) to Table (15) for different combinations of sample size n and a number of stages m. Further, the first column represents the lower bound confidence interval, the second column represents the upper bound of CI, the third column represents the average interval lengths (AILs), and in the last column, related coverage probabilities (CPs) in percentage (%).

From the results Tables [(3)-(8)] we observed the following:

- 1. The MSE of MLE and BE of the considered parameters decrease as the sample size increases.
- 2. For the same sample size, the average estimate for MLE tends to the initial values of the parameter with \$m\$ small.
- 3. For fixed n as m increasing the MLEs for scheme 5 and scheme 3 have the smallest and the largest MSE, respectively.
- 4. For fixed *n* as *m* increasing, the BEs for scheme 1 and scheme 5 have the smallest and the largest MSE, respectively.
- 5. For fixed *n*, the MSE of all estimates decreases for all cases as expected with *m* increasing.
- 6. The BEs of  $\beta_{11}$ ,  $\beta_{12}$ ,  $\beta_{21}$  and  $\beta_{22}$  under LINEX loss function ( $\nu = -0.5$ ) have the smallest MSEs as compared with estimates under the SE loss function and LINEX loss function ( $\nu = 0.5$ ).



- 7. The BEs of  $\alpha_1$  and  $\alpha_2$  under LINEX loss function ( $\nu = 0.5$ ) have the smallest MSEs compared to estimates under the SE loss function, LINEX loss function ( $\nu = -0.5$ ).
- 8. For the complete sample, the MLE and the BEs have the smallest MSE for all cases of progressive censored samples.

Now we compare the average lengths of different confidence/credible intervals. From tables Tables [(10)-(15)], we can see that

- 1. The length of approximate and credible CIs decreases as the sample size increases.
- 2. For *n* increasing, the coverage probability of credible CIs is greater than the coverage probability of approximate.
- 3. For fixed sample size and m small, the AIL for BE is shorter than the AIL for MLE using MCMC, but in most cases, for *m* increasing and fixed sample size, the AIL for MLE is shorter than the AIL for BEs.

From tables Tables [ (17)-(18)], the point and the interval estimates of the parameters  $\alpha_2$ ,  $\beta_{11}$ ,  $\beta_{21}$ ,  $\beta_{22}$  for BEs are better than for MLEs and the opposite is true for the parameter  $\alpha_1$ ,  $\beta_{12}$ .

A comparison of Bayesian estimation under MCMC for all different combinations of sample size n and number of stages m in the case of Scheme 3  $(S_3)$  can be shown graphically The graphs of MCMC estimates for  $\beta_{11}, \beta_{12}, \beta_{21}, \beta_{22}, \alpha_1$  and  $\alpha_2$  using MH algorithm in cases of informative priors are the plotting of estimates, histogram of estimates, and cumulative mean of estimates. These graphs can be shown in Figure (2) to Figure (4). Also, one can conclude the convergence of estimates under different sample sizes n and the number of stages m.6.

# 7. An Illustrative Example

In this section, we simulate progressive Type-II censored samples under step-stress for Nadarajah-Haghighi (NH) distribution in the presence of a competing failure model. The dataset is generated with the following choices of the parameters:  $\beta_{11} = 1.75$ ,  $\beta_{12} = 1.80$ ,  $\beta_{21} = 1.65$ ,  $\beta_{22} = 1.70$ ,  $\alpha_1 = 1.20$ , and  $\alpha_2 = 1.25$  and sample size n = 50, number of stages m = 30 with censoring scheme:

Assumed stress level as  $\tau = 0.5$ . The progressively censored Type-II data are given in the following Table.

<b>Table 2.</b> The progressive	very censored Type-II data for an illustrative example
First stress level	$\begin{array}{l} (0.004495655,1) \ (0.016194236,2) \ (0.024350506,2) \ (0.025145763,2) \\ (0.040138486,2) \ (0.042180897,2) \\ (0.053862568,2) \ (0.056847359,2) \ (0.066305768,2) \ (0.080662693,2) \\ (0.166929521,2) \ (0.176958457,2) \\ (0.178563050,2) \ (0.184591355,2) \ (0.192786798,2) \ (0.208997088,2) \\ \end{array}$
	(0.218379489,1)
Second stress	(0.2704664,2) (0.2837838,2) (0.3066917,2) (0.3290515,1) (0.3425723,1)
level	(0.3615052,1) $(0.3680463,1)$ $(0.3768950,1)$ $(0.3991376,1)$ $(0.4032060,1)$
	(0.4996059,1) (0.7712304,2) (0.7822973,1)

Table 7 Th d Tr II data for an illustration

The first element represents failure time and the second element represents the cause of failure.

From this data set, the estimates (Est.) and standard error (St.Er) of MLEs and BEs using MCMC of the parameters are derived. Also, Asy-CI and HPD intervals are computed. The results are presented in Table (17) for Est. and St.Ers and in Table (18) for Cis (lower, upper, interval length (IL)).





**Figure 2.** Convergence of MCMC estimates for  $\beta_{11}$  and  $\beta_{12}$  for n = 60 and m = 30

**Figure 3.** Convergence of MCMC estimates for  $\beta_{21}$  and  $\beta_{22}$  for n = 60 and m = 30



**Figure 4.** Convergence of MCMC estimates for  $\alpha_1$  and  $\alpha_2$  for n = 60 and m = 30

**Table 3.** Avg. estimated values and MSEs of the ML and BE using MCMC for different schemes (Sch.) and parameters (Parm.) of progressive Type-II censoring step-stress for NH distribution at n = 60 and m = 30

		MLE		DEMO	DE MCMC, SEI		<b>BE MCMC: LINEX</b>				
Sch.	Parm.			DE NIC	MC: SEL	v = -0	5	v = 0.5			
		Avg.	MSE	Avg.	MSE	Avg.	MSE	Avg.	MSE		
	α <sub>1</sub>	1.5257	0.0750	1.0918	0.1485	1.0604	0.1681	1.1296	0.1297		
<i>S</i> <sub>1</sub>	$\alpha_2$	1.5290	0.0792	1.0822	0.1938	1.0522	0.2162	1.1183	0.1709		
	$\beta_{11}$	0.2886	0.0068	0.5098	0.0798	0.4974	0.0724	0.5233	0.0884		
	$\beta_{12}$	0.2903	0.0150	0.5126	0.1099	0.5005	0.1014	0.5259	0.1196		
	$\beta_{21}$	0.6295	0.1064	1.2730	0.6596	1.1639	0.4883	1.4259	0.9540		
	$\beta_{22}$	0.6437	0.1656	1.2875	0.7623	1.1782	0.5774	1.4392	1.0693		
	α <sub>1</sub>	1.5010	0.0643	0.9817	0.2396	0.9476	0.2687	1.0235	0.2095		
	$\alpha_2$	1.5377	0.1011	0.9822	0.2918	0.9478	0.3239	1.0248	0.2577		
c	$\beta_{11}$	0.2997	0.0113	0.5879	0.1319	0.5696	0.1180	0.6086	0.1487		
<b>3</b> <sub>2</sub>	$\beta_{12}$	0.2932	0.0153	0.5887	0.1694	0.5701	0.1533	0.6098	0.1889		
	$\beta_{21}$	0.5938	0.1203	1.2674	0.6496	1.1619	0.4857	1.4137	0.9228		
	$\beta_{22}$	0.5819	0.1071	1.2733	0.7432	1.1665	0.5636	1.4220	1.0428		
<i>S</i> <sub>3</sub>	α <sub>1</sub>	1.5114	0.0922	1.0865	0.1536	1.0519	0.1753	1.1283	0.1336		



		MIE		DE MC	DE MCMC, SEI		BE MCMC: LINEX				
Sch.	Parm.	IVII	L.	BE MC	MC: SEL	v = -0	. 5	v = 0.5			
		Avg.	MSE	Avg.	MSE	Avg.	MSE	Avg.	MSE		
	α2	1.5280	0.1027	1.0881	0.1914	1.0538	0.2166	1.1295	0.1661		
	$\beta_{11}$	0.2966	0.0095	0.4948	0.0704	0.4837	0.0643	0.5068	0.0774		
	$\beta_{12}$	0.2945	0.0169	0.4927	0.0963	0.4819	0.0893	0.5045	0.1044		
	$\beta_{21}$	0.6783	0.1822	1.2708	0.6503	1.1630	0.4834	1.4201	0.9300		
	$\beta_{22}$	0.6775	0.2122	1.2675	0.7368	1.1612	0.5587	1.4185	1.0573		
	$\alpha_1$	1.5012	0.0698	1.0376	0.1911	1.0015	0.2182	1.0816	0.1633		
	α2	1.5168	0.0948	1.0381	0.2322	1.0019	0.2633	1.0824	0.1997		
c	$\beta_{11}$	0.2942	0.0080	0.5314	0.0923	0.5171	0.0832	0.5473	0.1031		
34	$\beta_{12}$	0.2934	0.0153	0.5299	0.1209	0.5155	0.1104	0.5457	0.1331		
	$\beta_{21}$	0.6511	0.1142	1.2819	0.6742	1.1752	0.5045	1.4282	0.9534		
	$\beta_{22}$	0.6560	0.1498	1.2790	0.7468	1.1712	0.5658	1.4287	1.0473		
	α <sub>1</sub>	1.5156	0.0811	0.9652	0.2630	0.9276	0.2954	1.0112	0.2293		
	α2	1.5539	0.0976	0.9671	0.3100	0.9288	0.3468	1.0147	0.2715		
c	$\beta_{11}$	0.2950	0.0078	0.5961	0.1366	0.5762	0.1212	0.6188	0.1553		
35	$\beta_{12}$	0.2868	0.0125	0.5972	0.1759	0.5773	0.1585	0.6198	0.1968		
	$\beta_{21}$	0.5825	0.0652	1.2602	0.6529	1.1571	0.4890	1.4033	0.9278		
	$\beta_{22}$	0.5668	0.0656	1.2527	0.7063	1.1496	0.5370	1.3961	0.9879		

**Table 4.** Avg. estimated values and MSEs of the ML and BE using MCMC for different schemes of progressive Type-II censoring step-stress for NH distribution at n = 60 and m = 40

		М		DE MON	IC. SEI		BE MCM	C: LINEX	K
Sch.	Parm.	IVL	LE	BE MCN	AC: SEL	v = -0.5	5	v = 0.5	
		Avg.	MSE	Avg.	MSE	Avg.	MSE	Avg.	MSE
	α <sub>1</sub>	1.4951	0.0662	1.0966	0.1457	1.0657	0.1641	1.1343	0.1286
	$\alpha_2$	1.5181	0.1246	1.1043	0.1797	1.0747	0.1996	1.1390	0.1603
c	$\beta_{11}$	0.2901	0.0074	0.4903	0.0671	0.4797	0.0613	0.5017	0.0736
<b>3</b> <sub>1</sub>	$\beta_{12}$	0.2887	0.0143	0.4846	0.0905	0.4744	0.0841	0.4955	0.0978
	$\beta_{21}$	0.6482	0.1409	1.2668	0.6574	1.1611	0.4898	1.4116	0.9348
	$\beta_{22}$	0.6495	0.1693	1.2450	0.7010	1.1437	0.5343	1.3826	0.9710
	α <sub>1</sub>	1.4784	0.0491	1.0239	0.2032	0.9909	0.2277	1.0644	0.1791
	α2	1.4961	0.0761	1.0177	0.2556	0.9852	0.2830	1.0574	0.2277
c	$\beta_{11}$	0.2906	0.0059	0.5347	0.0923	0.5211	0.0837	0.5496	0.1023
<b>3</b> <sub>2</sub>	$\beta_{12}$	0.2908	0.0145	0.5375	0.1256	0.5240	0.1157	0.5521	0.1370
	$\beta_{21}$	0.5944	0.0562	1.2618	0.6466	1.1583	0.4852	1.4035	0.9132
	$\beta_{22}$	0.6042	0.1213	1.2730	0.7449	1.1702	0.5719	1.4113	1.0201
	α <sub>1</sub>	1.4866	0.0804	1.0805	0.1565	1.0492	0.1773	1.1183	0.1356
	α2	1.4927	0.0965	1.0876	0.1935	1.0556	0.2167	1.1264	0.1706
c	$\beta_{11}$	0.2902	0.0076	0.4774	0.0590	0.4678	0.0542	0.4877	0.0644
33	$\beta_{12}$	0.2915	0.0153	0.4751	0.0840	0.4657	0.0783	0.4853	0.0904
	$\beta_{21}$	0.6701	0.1469	1.3163	1.3044	1.1718	0.5008	1.4246	0.9578
	$\beta_{22}$	0.6815	0.1968	1.2649	0.7252	1.1714	0.6091	1.4095	1.0125
	α1	1.5029	0.0674	1.1046	0.1417	1.0722	0.1607	1.1434	0.1237
	α2	1.5139	0.0758	1.1065	0.1747	1.0752	0.1965	1.1437	0.1529
S	$\beta_{11}$	0.2874	0.0064	0.4787	0.0619	0.4690	0.0568	0.4892	0.0676
34	$\beta_{12}$	0.2875	0.0140	0.4741	0.0845	0.4648	0.0788	0.4840	0.0908
	$\beta_{21}$	0.6361	0.1150	1.2416	0.6145	1.1400	0.4605	1.3812	0.8691
	$\beta_{22}$	0.6421	0.1471	1.2252	0.6630	1.1278	0.5082	1.3573	0.9124



	Parm.	MLE		DE MCI	AC. SEI	<b>BE MCMC: LINEX</b>			
Sch.				DE NICI	NC: SEL	v = -0.5		v = 0.5	
		Avg.	MSE	Avg.	MSE	Avg.	MSE	Avg.	MSE
	α <sub>1</sub>	1.5019	0.0484	0.9969	0.2279	0.9641	0.2545	1.0361	0.2005
	α2	1.5275	0.0779	1.0121	0.2656	0.9748	0.2964	1.0595	0.2363
c	$\beta_{11}$	0.2853	0.0046	0.5506	0.1035	0.5359	0.0937	0.5668	0.1150
35	$\beta_{12}$	0.2848	0.0125	0.5458	0.1323	0.5308	0.1209	0.5622	0.1455
	$\beta_{21}$	0.5778	0.0375	1.2636	0.6475	1.1639	0.4914	1.3993	0.9010
	$\beta_{22}$	0.5838	0.0712	1.2528	0.7076	1.1509	0.5397	1.3921	0.9824

**Table 5.** Avg. estimated values and MSEs of the ML and BE using MCMC for different schemes of progressive Type-II censoring step-stress for NH distribution at n = 80 and m = 40

		М	I TF	DE MCI	AC. SEI	]	BE MCM	C: LINEX	
Sch.	Parm.	IVI	LE	BE MC	NC: SEL	v = -0.5		v = 0.5	
		Avg.	MSE	Avg.	MSE	Avg.	MSE	Avg.	MSE
	α <sub>1</sub>	1.5212	0.0801	1.0984	0.1441	1.0676	0.1622	1.1361	0.1280
	$\alpha_2$	1.5396	0.0950	1.1033	0.1799	1.0728	0.2005	1.1395	0.1602
c	$\beta_{11}$	0.2846	0.0064	0.4901	0.0673	0.4797	0.0617	0.5014	0.0738
<b>3</b> <sub>1</sub>	$\beta_{12}$	0.2833	0.0132	0.4894	0.0957	0.4788	0.0887	0.5009	0.1038
	$\beta_{21}$	0.6134	0.0800	1.2479	0.6248	1.1461	0.4690	1.3876	0.8829
	$\beta_{22}$	0.6156	0.1145	1.2429	0.7011	1.1409	0.5334	1.3821	0.9731
	α <sub>1</sub>	1.5206	0.0704	1.0047	0.2223	0.9686	0.2506	1.0501	0.1945
	α2	1.5271	0.0708	1.0049	0.2694	0.9694	0.3007	1.0490	0.2370
c	$\beta_{11}$	0.2896	0.0150	0.5568	0.1090	0.5415	0.0983	0.5738	0.1215
<b>3</b> <sub>2</sub>	$\beta_{12}$	0.2884	0.0138	0.5561	0.1406	0.5410	0.1288	0.5727	0.1542
	$\beta_{21}$	0.5869	0.2473	1.2649	0.6506	1.1623	0.4901	1.4056	0.9136
	$\beta_{22}$	0.5887	0.1275	1.2596	0.7161	1.1577	0.5470	1.3998	0.9966
	α <sub>1</sub>	1.5176	0.0970	1.0945	0.1475	1.0613	0.1681	1.1345	0.1275
	α2	1.5225	0.0949	1.0912	0.1890	1.0593	0.2118	1.1295	0.1666
c	$\beta_{11}$	0.2898	0.0090	0.4716	0.0568	0.4628	0.0525	0.4810	0.0616
33	$\beta_{12}$	0.2894	0.0152	0.4711	0.0807	0.4624	0.0757	0.4804	0.0864
	$\beta_{21}$	0.6672	0.2007	1.2526	0.6345	1.1507	0.4748	1.4011	1.0493
	$\beta_{22}$	0.6695	0.2081	1.2494	0.7019	1.1507	0.5393	1.3843	0.9659
	α1	1.4865	0.0715	1.0403	0.1902	1.0051	0.2154	1.0833	0.1653
	$\alpha_2$	1.5383	0.1329	1.0305	0.2429	0.9967	0.2714	1.0712	0.2136
c	$\beta_{11}$	0.2907	0.0078	0.5085	0.0766	0.4967	0.0699	0.5214	0.0845
34	$\beta_{12}$	0.2848	0.0143	0.5139	0.1083	0.5019	0.1001	0.5269	0.1176
	$\beta_{21}$	0.6414	0.0982	1.2595	0.6367	1.1590	0.4807	1.3972	0.8932
	$\beta_{22}$	0.6354	0.1448	1.2795	0.7584	1.1767	0.5829	1.4189	1.0383
	α <sub>1</sub>	1.5104	0.0565	0.9605	0.2629	0.9241	0.2949	1.0054	0.2298
	α2	1.5576	0.0744	0.9602	0.3180	0.9233	0.3533	1.0062	0.2813
S-	$\beta_{11}$	0.2888	0.0052	0.5817	0.1237	0.5644	0.1112	0.6009	0.1386
55	$\beta_{12}$	0.2804	0.0099	0.5865	0.1654	0.5687	0.1504	0.6063	0.1831
	$\beta_{21}$	0.5638	0.0395	1.2480	0.6218	1.1505	0.4718	1.3790	0.8611
	$\beta_{22}$	0.5466	0.0423	1.2540	0.7114	1.1542	0.5459	1.3908	0.9814



		М	IF	DE MCI	AC. SEI	]	BE MCM	C: LINEX	
Sch.	Parm.	IVI.	LE	BE MU	NC: SEL	v = -0.5	)	v = 0.5	
		Avg.	MSE	Avg.	MSE	Avg.	MSE	Avg.	MSE
	α1	1.5166	0.0702	1.1209	0.1292	1.0921	0.1448	1.1555	0.1153
	$\alpha_2$	1.5308	0.0931	1.1167	0.1706	1.0891	0.1886	1.1490	0.1529
c	$\beta_{11}$	0.2784	0.0050	0.4559	0.0487	0.4483	0.0452	0.4639	0.0524
<b>3</b> <sub>1</sub>	$\beta_{12}$	0.2789	0.0113	0.4599	0.0750	0.4521	0.0706	0.4682	0.0799
	$\beta_{21}$	0.6077	0.0794	1.1942	0.5462	1.1065	0.4186	1.3098	0.7460
	$\beta_{22}$	0.6186	0.1246	1.2064	0.6458	1.1161	0.5012	1.3279	0.8775
	α1	1.4882	0.0624	1.0703	0.1697	1.0389	0.1896	1.1078	0.1512
	$\alpha_2$	1.5018	0.0770	1.0630	0.2158	1.0324	0.2388	1.0995	0.1929
c	$\beta_{11}$	0.2917	0.0096	0.4952	0.0679	0.4851	0.0625	0.5061	0.0740
32	$\beta_{12}$	0.2902	0.0149	0.4990	0.0990	0.4892	0.0926	0.5094	0.1060
	$\beta_{21}$	0.6127	0.2074	1.2015	0.5619	1.1110	0.4287	1.3239	0.7789
	$\beta_{22}$	0.6100	0.1596	1.2058	0.6403	1.1168	0.4979	1.3235	0.8628
	α <sub>1</sub>	1.5008	0.0619	1.1054	0.1373	1.0758	0.1550	1.1404	0.1203
	$\alpha_2$	1.5142	0.0817	1.1125	0.1736	1.0826	0.1934	1.1481	0.1546
c	$\beta_{11}$	0.2836	0.0058	0.4584	0.0494	0.4509	0.0459	0.4664	0.0532
33	$\beta_{12}$	0.2838	0.0126	0.4575	0.0736	0.4499	0.0694	0.4655	0.0783
	$\beta_{21}$	0.6168	0.0811	1.2027	0.5551	1.1133	0.4244	1.3211	0.7617
	$\beta_{22}$	0.6269	0.1306	1.1918	0.6179	1.1031	0.4779	1.3210	0.9516
	α <sub>1</sub>	1.5121	0.0776	1.1225	0.1300	1.0942	0.1451	1.1555	0.1160
	$\alpha_2$	1.5315	0.0857	1.1183	0.1685	1.0888	0.1872	1.1536	0.1509
c	$\beta_{11}$	0.2809	0.0056	0.4511	0.0461	0.4439	0.0429	0.4587	0.0496
34	$\beta_{12}$	0.2794	0.0119	0.4561	0.0722	0.4486	0.0681	0.4640	0.0766
	$\beta_{21}$	0.6156	0.0999	1.1804	0.5272	1.0951	0.4052	1.2926	0.7170
	$\beta_{22}$	0.6182	0.1448	1.1942	0.6169	1.1057	0.4798	1.3114	0.8307
	α <sub>1</sub>	1.4948	0.0490	1.0334	0.1972	1.0011	0.2203	1.0727	0.1745
	$\alpha_2$	1.5020	0.0587	1.0245	0.2512	0.9919	0.2776	1.0645	0.2254
S	$\beta_{11}$	0.2866	0.0050	0.5189	0.0821	0.5074	0.0753	0.5313	0.0898
35	$\beta_{12}$	0.2879	0.0138	0.5253	0.1165	0.5136	0.1083	0.5378	0.1258
	$\beta_{21}$	0.5685	0.0397	1.2109	0.5766	1.1198	0.4394	1.3331	0.7975
	$\beta_{22}$	0.5745	0.0683	1.2272	0.6623	1.1348	0.5158	1.3481	0.8861

**Table 6.** Avg. estimated values and MSEs of the ML and BE using MCMC for different schemes of progressive Type-II censoring step-stress for NH distribution at n = 80 and m = 60

**Table 7.** Avg. estimated values and MSEs of the ML and BE using MCMC for different schemes of progressive Type-II censoring step-stress for NH distribution at n = 100 and m = 60

		MLE		DE MCI	AC, SEI	<b>BE MCMC: LINEX</b>			
Sch.	Parm.			DE NICI	IC: SEL	v = -0.5		v = 0.5	
		Avg.	MSE	Avg.	MSE	Avg.	MSE	Avg.	MSE
	α <sub>1</sub>	1.5105	0.0830	1.1051	0.1418	1.0787	0.1567	1.1354	0.1277
	$\alpha_2$	1.5212	0.0851	1.1255	0.1654	1.0961	0.1835	1.1602	0.1484
c	$\beta_{11}$	0.2837	0.0065	0.4657	0.0530	0.4578	0.0492	0.4742	0.0572
<b>3</b> <sub>1</sub>	$\beta_{12}$	0.2826	0.0125	0.4594	0.0741	0.4514	0.0697	0.4678	0.0790
	$\beta_{21}$	0.6327	0.1484	1.2219	0.5962	1.1308	0.4565	1.3465	0.8287
	$\beta_{22}$	0.6281	0.1423	1.1933	0.6221	1.1034	0.4809	1.3162	0.8548



	<b>D</b>	м	F	<b>BE MCN</b>	AC: SFI	BE MCMC: LINEX			
Sch.	Parm.	191		DE MC	IC. SEL	<i>v</i> = -	0.5	v = 0.5	
		Avg.	MSE	Avg.	MSE	Avg.	MSE	Avg.	MSE
	α <sub>1</sub>	1.4943	0.0571	1.0294	0.2016	0.9975	0.2246	1.0685	0.1792
	$\alpha_2$	1.5100	0.0737	1.0228	0.2531	0.9914	0.2790	1.0604	0.2269
c	$\beta_{11}$	0.2863	0.0052	0.5183	0.0821	0.5070	0.0754	0.5304	0.0898
<b>3</b> <sub>2</sub>	$\beta_{12}$	0.2862	0.0127	0.5217	0.1134	0.5105	0.1057	0.5337	0.1221
	$\beta_{21}$	0.5750	0.0523	1.2113	0.5755	1.1269	0.4575	1.3292	0.7846
	$\beta_{22}$	0.5784	0.0789	1.2279	0.6893	1.1360	0.5308	1.3554	1.0191
	$\alpha_1$	1.5082	0.0870	1.1151	0.1342	1.0847	0.1515	1.1510	0.1178
	$\alpha_2$	1.5144	0.1042	1.1184	0.1687	1.0871	0.1893	1.1559	0.1485
6	$\beta_{11}$	0.2810	0.0057	0.4436	0.0434	0.4369	0.0405	0.4506	0.0465
33	$\beta_{12}$	0.2819	0.0120	0.4432	0.0647	0.4364	0.0611	0.4505	0.0686
	$\beta_{21}$	0.6316	0.0971	1.1847	0.5314	1.0999	0.4095	1.2952	0.7194
	$\beta_{22}$	0.6396	0.1357	1.1857	0.6065	1.0984	0.4718	1.3067	0.8312
	α1	1.5105	0.0798	1.1148	0.1352	1.0854	0.1513	1.1498	0.1207
	$\alpha_2$	1.5143	0.0936	1.1162	0.1671	1.0858	0.1879	1.1523	0.1466
c	$\beta_{11}$	0.2847	0.0063	0.4530	0.0473	0.4460	0.0442	0.4605	0.0508
34	$\beta_{12}$	0.2860	0.0131	0.4547	0.0712	0.4472	0.0670	0.4626	0.0759
	$\beta_{21}$	0.6243	0.1060	1.1773	0.5265	1.0944	0.4068	1.2873	0.7171
	$\beta_{22}$	0.6349	0.1433	1.1860	0.6133	1.0978	0.4743	1.3046	0.8375
	α1	1.4968	0.0441	0.9991	0.2316	0.9642	0.2585	1.0414	0.2047
	$\alpha_2$	1.5467	0.0896	1.0069	0.2712	0.9709	0.3021	1.0516	0.2402
c	$\beta_{11}$	0.2837	0.0044	0.5395	0.0946	0.5264	0.0863	0.5536	0.1039
35	$\beta_{12}$	0.2774	0.0100	0.5359	0.1249	0.5227	0.1152	0.5503	0.1360
	$\beta_{21}$	0.5702	0.0347	1.2472	0.6362	1.1523	0.4867	1.3733	0.8716
	$\beta_{22}$	0.5626	0.0565	1.2323	0.6824	1.1391	0.5306	1.3571	0.9226

**Table 8.** Avg. estimated values and MSEs of the ML and BE using MCMC for different schemes of progressive Type-II censoring step-stress for NH distribution at n = 100 and m = 80

		м	[ F	DE MCI	AC. SEI	]	BE MCM	C: LINEX	
Sch.	Parm.	IVI		DE NICI	AC: SEL	v = -	- <b>0</b> . 5	<i>v</i> =	0.5
		Avg.	MSE	Avg.	MSE	Avg.	MSE	Avg.	MSE
	α <sub>1</sub>	1.4890	0.0634	1.1435	0.1176	1.1160	0.1310	1.1756	0.1056
	$\alpha_2$	1.5003	0.0739	1.1439	0.1520	1.1159	0.1681	1.1767	0.1371
c	$\beta_{11}$	0.2856	0.0070	0.4385	0.0416	0.4322	0.0390	0.4452	0.0445
$\mathbf{s}_1$	$\beta_{12}$	0.2841	0.0126	0.4390	0.0627	0.4328	0.0595	0.4456	0.0661
	$\beta_{21}$	0.6291	0.1252	1.1383	0.4796	1.0609	0.3717	1.2411	0.6506
	$\beta_{22}$	0.6287	0.1470	1.1392	0.5485	1.0633	0.4352	1.2367	0.7184
	α <sub>1</sub>	1.4935	0.0587	1.0809	0.1633	1.0508	0.1814	1.1170	0.1467
	$\alpha_2$	1.5106	0.0699	1.0906	0.1942	1.0591	0.2153	1.1283	0.1748
c	$\beta_{11}$	0.2824	0.0051	0.4772	0.0597	0.4688	0.0555	0.4861	0.0643
<b>3</b> <sub>2</sub>	$\beta_{12}$	0.2811	0.0118	0.4726	0.0814	0.4643	0.0765	0.4815	0.0868
	$\beta_{21}$	0.5864	0.0716	1.1857	0.5529	1.0991	0.4235	1.3006	0.7594
	$\beta_{22}$	0.5893	0.1075	1.1674	0.5920	1.0825	0.4597	1.2794	0.8007
C C	α <sub>1</sub>	1.4863	0.0780	1.1358	0.1266	1.1087	0.1401	1.1669	0.1143
<i>S</i> <sub>3</sub>	$\alpha_2$	1.4898	0.0841	1.1320	0.1606	1.1033	0.1781	1.1661	0.1440



		м	IF	DE MC	RF MCMC· SFI		BE MCMC: LINEX				
Sch.	Parm.	IVI.	LE	DE NICI	NC: SEL	v = -	- <b>0</b> . 5	<i>v</i> =	0.5		
		Avg.	MSE	Avg.	MSE	Avg.	MSE	Avg.	MSE		
	$\beta_{11}$	0.2867	0.0067	0.4363	0.0402	0.4303	0.0378	0.4425	0.0428		
	$\beta_{12}$	0.2882	0.0141	0.4393	0.0627	0.4330	0.0595	0.4458	0.0661		
	$\beta_{21}$	0.6431	0.1470	1.1427	0.4903	1.0676	0.3839	1.2398	0.6527		
	$\beta_{22}$	0.6552	0.1932	1.1552	0.5701	1.0772	0.4520	1.2551	0.7448		
	α1	1.5167	0.0752	1.1359	0.1214	1.1088	0.1355	1.1671	0.1082		
c	α2	1.5178	0.0777	1.1393	0.1551	1.1110	0.1716	1.1728	0.1398		
	$\beta_{11}$	0.2747	0.0042	0.4353	0.0391	0.4292	0.0366	0.4418	0.0417		
34	$\beta_{12}$	0.2771	0.0108	0.4349	0.0606	0.4288	0.0576	0.4412	0.0639		
	$\beta_{21}$	0.6012	0.0821	1.1541	0.5043	1.0751	0.3915	1.2581	0.6816		
	$\beta_{22}$	0.6163	0.1345	1.1496	0.5619	1.0717	0.4442	1.2500	0.7389		
	α <sub>1</sub>	1.4921	0.0503	1.0727	0.1743	1.0392	0.1938	1.1135	0.1578		
	$\alpha_2$	1.5119	0.0637	1.0656	0.2119	1.0334	0.2363	1.1042	0.1876		
c	$\beta_{11}$	0.2831	0.0047	0.4874	0.0654	0.4783	0.0606	0.4972	0.0707		
35	$\beta_{12}$	0.2814	0.0112	0.4885	0.0906	0.4792	0.0849	0.4985	0.0970		
	$\beta_{21}$	0.5775	0.0493	1.1811	0.5374	1.0970	0.4149	1.2914	0.7279		
	$\beta_{22}$	0.5814	0.0882	1.1846	0.6055	1.0981	0.4724	1.2990	0.8139		

**Table 9.** Avg. estimated values and MSEs of the ML and BE using MCMC at complete sampling step-stress for NH distribution at n = 60, 80 and n = 100

		м	[ F	DE MCI	AC. SEI	]	BE MCM	C: LINEX	Κ
n	Parm.	IVL	LE	BE MC	NC: SEL	v = -	-0.5	<i>v</i> =	0.5
		Avg.	MSE	Avg.	MSE	Avg.	MSE	Avg.	MSE
	α <sub>1</sub>	1.5123	0.0708	1.1304	0.1265	1.1008	0.1412	1.1657	0.1152
	$\alpha_2$	1.5252	0.0935	1.1137	0.1716	1.0871	0.1889	1.1446	0.1547
(0)	$\beta_{11}$	0.2807	0.0060	0.4524	0.0471	0.4450	0.0438	0.4603	0.0507
00	$\beta_{12}$	0.2808	0.0124	0.4585	0.0732	0.4510	0.0691	0.4665	0.0778
	$\beta_{21}$	0.6168	0.1007	1.1778	0.5196	1.0915	0.3974	1.2923	0.7142
	$\beta_{22}$	0.6260	0.1648	1.2001	0.6320	1.1133	0.4948	1.3165	0.8492
	α <sub>1</sub>	1.4996	0.0658	1.1379	0.1223	1.1106	0.1357	1.1696	0.1103
	$\alpha_2$	1.5076	0.0850	1.1438	0.1520	1.1156	0.1682	1.1771	0.1377
90	$\beta_{11}$	0.2815	0.0051	0.4431	0.0437	0.4366	0.0409	0.4500	0.0468
00	$\beta_{12}$	0.2832	0.0122	0.4398	0.0636	0.4334	0.0602	0.4466	0.0672
	$\beta_{21}$	0.6012	0.0745	1.1310	0.4623	1.0547	0.3595	1.2311	0.6227
	$\beta_{22}$	0.6140	0.1165	1.1244	0.5231	1.0491	0.4145	1.2229	0.6900
	α <sub>1</sub>	1.5110	0.0674	1.1539	0.1173	1.1277	0.1288	1.1842	0.1074
	$\alpha_2$	1.5282	0.0791	1.1585	0.1448	1.1317	0.1588	1.1898	0.1329
100	$\beta_{11}$	0.2768	0.0049	0.4272	0.0369	0.4218	0.0348	0.4329	0.0391
100	$\beta_{12}$	0.2750	0.0103	0.4244	0.0555	0.4191	0.0529	0.4300	0.0582
	$\beta_{21}$	0.5973	0.0911	1.1019	0.4446	1.0357	0.3545	1.1855	0.5780
	$\beta_{22}$	0.5963	0.1171	1.0916	0.4872	1.0251	0.3907	1.1752	0.6284



Sch. Parm.		Asy	-CI		HPD				
501.	rarm.	Lower	Upper	AIL	CP (%)	Lower	Upper	AIL	CP (%)
	α1	1.0096	2.0418	1.0322	96.1	0.8225	1.3720	0.5495	96.0
	$\alpha_2$	0.9800	2.0779	1.0980	95.9	0.8481	1.3675	0.5195	97.5
c	$\beta_{11}$	0.1452	0.4319	0.2866	96.4	0.3055	0.7195	0.4140	95.6
$\mathbf{s}_1$	$\beta_{12}$	0.1280	0.4526	0.3246	96.0	0.3271	0.7311	0.4040	96.8
	$\beta_{21}$	0.0425	1.2165	1.1740	96.2	0.8014	1.7229	0.9215	96.4
	$\beta_{22}$	0.0000	1.3456	1.3456	96.5	0.8067	1.7385	0.9318	97.1
	$\alpha_1$	1.0139	1.9881	0.9742	97.0	0.7250	1.2625	0.5375	96.1
	$\alpha_2$	0.9188	2.1567	1.2379	97.4	0.7181	1.2803	0.5622	96.1
G	$\beta_{11}$	0.1153	0.4842	0.3689	97.4	0.3480	0.8266	0.4786	96.0
<b>S</b> <sub>2</sub>	$\beta_{12}$	0.1334	0.4529	0.3195	97.3	0.3462	0.8506	0.5044	96.3
	$\beta_{21}$	0.0000	1.2487	1.2487	98.3	0.7952	1.7345	0.9393	96.8
	$\beta_{22}$	0.0000	1.1693	1.1693	96.4	0.7705	1.7428	0.9722	97.4
	$\alpha_1$	0.9284	2.0944	1.1660	96.0	0.8355	1.3675	0.5320	96.3
	$\alpha_2$	0.9020	2.1540	1.2520	96.5	0.8183	1.3663	0.5480	96.5
c	$\beta_{11}$	0.1287	0.4644	0.3357	96.5	0.3071	0.6893	0.3822	96.3
<b>3</b> 3	$\beta_{12}$	0.1198	0.4693	0.3495	96.1	0.3217	0.7029	0.3811	96.4
	$\beta_{21}$	0.0000	1.4389	1.4389	97.1	0.8231	1.7147	0.8916	96.4
	$\beta_{22}$	0.0000	1.4629	1.4629	96.2	0.7900	1.7764	0.9864	96.8
	$\alpha_1$	0.9928	2.0096	1.0168	97.3	0.7837	1.3280	0.5443	96.3
	$\alpha_2$	0.9140	2.1195	1.2055	97.1	0.7992	1.3299	0.5307	97.4
c	$\beta_{11}$	0.1421	0.4463	0.3042	95.2	0.3425	0.7548	0.4123	96.3
34	$\beta_{12}$	0.1350	0.4518	0.3168	96.2	0.3296	0.7391	0.4095	95.7
	$\beta_{21}$	0.0585	1.2438	1.1853	96.7	0.8029	1.7595	0.9567	96.2
	$\beta_{22}$	0.0134	1.2986	1.2852	96.4	0.8590	1.7497	0.8907	97.6
	$\alpha_1$	0.9722	2.0589	1.0867	96.2	0.6865	1.3103	0.6237	96.2
	$\alpha_2$	0.9503	2.1575	1.2072	96.6	0.6966	1.3009	0.6043	96.1
c	$\beta_{11}$	0.1464	0.4436	0.2972	96.6	0.3744	0.8431	0.4688	97.0
35	$\beta_{12}$	0.1489	0.4248	0.2759	97.0	0.3484	0.8312	0.4829	95.7
	$\beta_{21}$	0.1087	1.0563	0.9476	97.7	0.7624	1.8282	1.0658	97.0
	$\beta_{22}$	0.1201	1.0136	0.8935	96.6	0.7807	1.7331	0.9523	96.5

**Table 10.** Interval estimates, AILs and CP(%) values of the ML and BE using MCMC for different schemes of progressive Type-II step-stress for NH distribution at n = 60 and m = 30

**Table 11.** Interval estimates, AILs and CP(%) values of the ML and BE using MCMC for different schemes of progressive Type-II step-stress for NH distribution at n = 60 and m = 40

Sch.	Donm		As	y-CI		HPD				
Scii.	rarm.	Lower	Upper	AIL	CP (%)	Lower	Upper	AIL	CP (%)	
	α1	0.9982	1.9919	0.9938	97.4	0.8491	1.3825	0.5334	96.1	
	$\alpha_2$	0.8268	2.2094	1.3826	97.8	0.8476	1.4023	0.5547	95.8	
c	$\beta_{11}$	0.1408	0.4394	0.2986	95.3	0.3262	0.6810	0.3548	97.1	
<b>3</b> <sub>1</sub>	$\beta_{12}$	0.1314	0.4459	0.3144	95.1	0.3135	0.6820	0.3685	97.3	
	$\beta_{21}$	0.0000	1.3244	1.3244	95.5	0.8381	1.8435	1.0055	98.5	
	$\beta_{22}$	0.0000	1.3551	1.3551	95.6	0.7905	1.8166	1.0261	98.1	
c	α <sub>1</sub>	1.0476	1.9093	0.8617	97.4	0.7796	1.3316	0.5521	96.9	
<b>3</b> <sub>2</sub>	α2	0.9551	2.0372	1.0821	98.5	0.7344	1.2955	0.5611	95.3	



Cab	Dawn		As	y-CI		HPD				
Scn.	Parm.	Lower	Upper	AIL	CP (%)	Lower	Upper	AIL	CP (%)	
	$\beta_{11}$	0.1632	0.4180	0.2549	96.1	0.3365	0.7229	0.3864	96.3	
	$\beta_{12}$	0.1357	0.4459	0.3102	96.5	0.3409	0.7433	0.4024	96.2	
	$\beta_{21}$	0.1682	1.0207	0.8525	97.0	0.7804	1.7697	0.9893	97.5	
	$\beta_{22}$	0.0000	1.2165	1.2165	97.7	0.7510	1.7810	1.0300	96.9	
	$\alpha_1$	0.9352	2.0379	1.1027	96.6	0.8255	1.3639	0.5384	96.3	
	$\alpha_2$	0.8837	2.1016	1.2180	96.8	0.8492	1.4023	0.5531	97.0	
c	$\beta_{11}$	0.1387	0.4416	0.3029	95.0	0.3112	0.6428	0.3315	96.4	
<b>3</b> 3	$\beta_{12}$	0.1280	0.4551	0.3271	94.5	0.3085	0.6500	0.3415	96.4	
	$\beta_{21}$	0.0000	1.3435	1.3435	95.8	0.7689	1.6926	0.9237	95.5	
	$\beta_{22}$	0.0000	1.4236	1.4236	96.1	0.8322	1.7614	0.9292	97.6	
	α <sub>1</sub>	1.0043	2.0015	0.9972	96.1	0.8255	1.3971	0.5716	95.6	
	$\alpha_2$	0.9746	2.0532	1.0786	96.5	0.8642	1.3730	0.5089	96.7	
c	$\beta_{11}$	0.1487	0.4261	0.2774	96.1	0.3196	0.7023	0.3826	97.4	
34	$\beta_{12}$	0.1309	0.4441	0.3132	95.8	0.3093	0.6747	0.3653	96.3	
	$\beta_{21}$	0.0268	1.2453	1.2185	96.0	0.8153	1.7675	0.9522	98.1	
	$\beta_{22}$	0.0000	1.2931	1.2931	95.6	0.7897	1.7073	0.9177	97.2	
	α <sub>1</sub>	1.0825	1.9213	0.8388	96.1	0.7312	1.2769	0.5457	96.3	
	α2	0.9829	2.0720	1.0891	95.5	0.7157	1.3185	0.6028	96.1	
c	$\beta_{11}$	0.1711	0.3994	0.2282	96.0	0.3447	0.7727	0.4280	96.3	
35	$\beta_{12}$	0.1415	0.4281	0.2865	96.2	0.3432	0.7643	0.4211	96.8	
	$\beta_{21}$	0.2301	0.9255	0.6954	95.7	0.8051	1.7721	0.9670	97.2	
	$\beta_{22}$	0.1312	1.0363	0.9051	95.5	0.7931	1.7514	0.9583	96.4	

**Table 12.** Interval estimates, AILs and CP(%) values of the ML and BE using MCMC for different schemes of progressive Type-II step-stress for NH distribution at n = 80 and m = 40

Sch.	Dowm		As	y-CI		HPD				
Scii.	rarm.	Lower	Upper	AIL	CP (%)	Lower	Upper	AIL	CP (%)	
	$\alpha_1$	0.9841	2.0582	1.0742	94.6	0.8573	1.4023	0.5450	97.0	
	$\alpha_2$	0.9401	2.1391	1.1990	96.1	0.8185	1.3714	0.5529	95.7	
c	$\beta_{11}$	0.1437	0.4254	0.2817	95.6	0.3254	0.6856	0.3602	97.0	
$\mathbf{s}_1$	$\beta_{12}$	0.1276	0.4390	0.3114	95.8	0.2981	0.7245	0.4264	96.1	
	$\beta_{21}$	0.1053	1.1216	1.0163	95.8	0.7313	1.7207	0.9894	96.4	
	$\beta_{22}$	0.0368	1.1943	1.1575	94.8	0.7552	1.7803	1.0251	97.5	
	α <sub>1</sub>	1.0191	2.0221	1.0030	96.6	0.7403	1.3208	0.5805	96.0	
	$\alpha_2$	1.0082	2.0460	1.0378	96.9	0.7128	1.2995	0.5867	95.8	
C	$\beta_{11}$	0.0627	0.5165	0.4538	99.5	0.3463	0.8160	0.4697	97.4	
<b>3</b> <sub>2</sub>	$\beta_{12}$	0.1366	0.4403	0.3037	97.3	0.3374	0.7956	0.4582	96.3	
	$\beta_{21}$	0.0000	1.5470	1.5470	99.7	0.7730	1.7377	0.9646	96.5	
	$\beta_{22}$	0.0000	1.2338	1.2338	97.2	0.7849	1.7167	0.9317	96.5	
	α <sub>1</sub>	0.9216	2.1136	1.1921	96.3	0.8468	1.3863	0.5395	96.5	
	$\alpha_2$	0.9200	2.1250	1.2050	96.6	0.8449	1.3896	0.5447	96.0	
C	$\beta_{11}$	0.1213	0.4582	0.3369	96.4	0.3124	0.6487	0.3363	96.4	
33	$\beta_{12}$	0.1224	0.4564	0.3340	95.4	0.3182	0.6378	0.3197	96.9	
	$\beta_{21}$	0.0000	1.4823	1.4823	96.6	0.7532	1.6851	0.9319	96.2	
	$\beta_{22}$	0.0000	1.4537	1.4537	95.3	0.7562	1.7212	0.9650	96.5	



Sah	Dowm		As	y-CI		HPD					
Scn.	rarm.	Lower	Upper	AIL	CP (%)	Lower	Upper	AIL	CP (%)		
	$\alpha_1$	0.9669	2.0061	1.0392	96.6	0.7636	1.3149	0.5513	95.4		
	$\alpha_2$	0.8274	2.2493	1.4218	97.4	0.7824	1.3468	0.5644	97.4		
c	$\beta_{11}$	0.1371	0.4444	0.3073	94.5	0.3419	0.7098	0.3680	96.7		
34	$\beta_{12}$	0.1189	0.4506	0.3317	95.9	0.3422	0.7033	0.3611	96.7		
	$\beta_{21}$	0.0930	1.1897	1.0967	96.0	0.8087	1.7184	0.9097	96.9		
	$\beta_{22}$	0.0000	1.2871	1.2871	96.0	0.7820	1.7523	0.9703	96.4		
	α <sub>1</sub>	1.0594	1.9613	0.9019	95.7	0.6827	1.2666	0.5839	96.6		
	α2	1.0349	2.0803	1.0453	95.7	0.6985	1.3158	0.6173	97.2		
c	$\beta_{11}$	0.1699	0.4078	0.2379	96.6	0.3686	0.8304	0.4619	96.9		
<b>3</b> 5	$\beta_{12}$	0.1647	0.3960	0.2314	97.2	0.3584	0.8355	0.4770	96.4		
	$\beta_{21}$	0.1945	0.9331	0.7386	97.0	0.7695	1.7339	0.9644	96.4		
	$\beta_{22}$	0.1905	0.9027	0.7122	95.2	0.7726	1.7411	0.9685	96.4		

**Table 13.** Interval estimates, AILs and CP(%) values of the ML and BE using MCMC for different schemes of progressive Type-II step-stress for NH distribution at n = 80 and m = 60

Sch.	Dorm		As	y-CI		HPD				
5cii.	1 al III.	Lower	Upper	AIL	CP (%)	Lower	Upper	AIL	CP (%)	
	α <sub>1</sub>	1.0139	2.0193	1.0055	95.9	0.8704	1.4061	0.5357	95.8	
	$\alpha_2$	0.9355	2.1261	1.1906	95.7	0.8587	1.4181	0.5593	96.0	
c	$\beta_{11}$	0.1509	0.4059	0.2549	95.1	0.3126	0.6013	0.2887	96.4	
<b>5</b> <sub>1</sub>	$\beta_{12}$	0.1397	0.4180	0.2783	94.3	0.3025	0.6161	0.3136	96.2	
	$\beta_{21}$	0.0972	1.1182	1.0210	95.4	0.7345	1.6924	0.9579	96.9	
	$\beta_{22}$	0.0104	1.2268	1.2163	95.5	0.7076	1.7118	1.0042	97.2	
	α <sub>1</sub>	1.0042	1.9722	0.9680	96.9	0.7759	1.3670	0.5911	95.4	
	$\alpha_2$	0.9576	2.0460	1.0884	96.6	0.7749	1.3501	0.5752	95.5	
c	$\beta_{11}$	0.1178	0.4656	0.3478	97.7	0.3352	0.6686	0.3334	96.7	
<b>3</b> <sub>2</sub>	$\beta_{12}$	0.1292	0.4511	0.3219	96.7	0.3271	0.6951	0.3680	96.7	
	$\beta_{21}$	0.0000	1.4779	1.4779	97.9	0.7185	1.7328	1.0143	98.1	
	$\beta_{22}$	0.0000	1.3277	1.3277	96.8	0.7499	1.7372	0.9873	98.1	
	α <sub>1</sub>	1.0232	1.9784	0.9552	96.5	0.8473	1.3661	0.5188	96.3	
	$\alpha_2$	0.9544	2.0739	1.1195	95.9	0.8480	1.4075	0.5595	96.4	
c.	$\beta_{11}$	0.1499	0.4173	0.2674	95.4	0.3271	0.6082	0.2811	96.6	
33	$\beta_{12}$	0.1370	0.4306	0.2936	95.1	0.2829	0.6150	0.3321	95.4	
	$\beta_{21}$	0.1074	1.1263	1.0188	95.6	0.7660	1.6923	0.9262	97.3	
	$\beta_{22}$	0.0089	1.2450	1.2361	95.8	0.7424	1.6981	0.9557	97.4	
	α <sub>1</sub>	0.9797	2.0444	1.0647	97.0	0.8904	1.4378	0.5474	96.9	
	α2	0.9608	2.1021	1.1413	96.3	0.8650	1.3969	0.5319	95.6	
c.	$\beta_{11}$	0.1473	0.4145	0.2672	96.2	0.3029	0.5889	0.2859	96.3	
34	$\beta_{12}$	0.1324	0.4264	0.2940	96.3	0.3035	0.6054	0.3018	96.6	
	$\beta_{21}$	0.0389	1.1924	1.1536	96.2	0.7172	1.6831	0.9659	97.9	
	$\beta_{22}$	0.0000	1.2874	1.2874	96.4	0.7393	1.6969	0.9576	97.6	
	$\alpha_1$	1.0698	1.9198	0.8499	97.3	0.7863	1.3387	0.5524	96.3	
<i>S</i> <sub>5</sub>	$\alpha_2$	1.0268	1.9773	0.9504	96.4	0.7392	1.3502	0.6109	96.1	
55	$\beta_{11}$	0.1681	0.4051	0.2370	96.5	0.3328	0.7187	0.3859	96.0	



Sah	Donm		As	y-CI		HPD				
Scii.	rarm.	Lower	Upper	AIL	CP (%)	Lower	Upper	AIL	CP (%)	
	$\beta_{12}$	0.1348	0.4411	0.3063	96.8	0.3326	0.7255	0.3929	96.5	
	$\beta_{21}$	0.2017	0.9353	0.7336	96.0	0.7365	1.7457	1.0091	96.7	
	$\beta_{22}$	0.1236	1.0253	0.9016	97.1	0.7639	1.6940	0.9301	96.9	

**Table 14.** Interval estimates, AILs and CP(%) values of the ML and BE using MCMC for different schemes of progressive Type-II step-stress for NH distribution at n = 100 and m = 60

	D		As	y-CI			Н	PD	
Scn.	Parm.	Lower	Upper	AIL	CP (%)	Lower	Upper	AIL	CP (%)
	α <sub>1</sub>	0.9581	2.0629	1.1047	96.6	0.8352	1.3717	0.5365	95.8
	$\alpha_2$	0.9508	2.0917	1.1409	96.4	0.8871	1.4780	0.5908	97.5
c	$\beta_{11}$	0.1405	0.4268	0.2863	94.9	0.3007	0.6150	0.3143	96.1
<b>3</b> <sub>1</sub>	$\beta_{12}$	0.1353	0.4299	0.2946	94.1	0.2949	0.6142	0.3192	96.4
	$\beta_{21}$	0.0000	1.3419	1.3419	96.2	0.7738	1.8401	1.0663	97.8
	$\beta_{22}$	0.0000	1.2802	1.2802	95.1	0.7463	1.7619	1.0156	98.0
	$\alpha_1$	1.0340	1.9546	0.9206	97.4	0.7579	1.3757	0.6179	96.9
	$\alpha_2$	0.9782	2.0418	1.0636	96.7	0.7832	1.3977	0.6145	97.5
S.	$\beta_{11}$	0.1638	0.4088	0.2450	96.2	0.3294	0.7123	0.3830	95.8
52	$\beta_{12}$	0.1433	0.4291	0.2858	96.6	0.3346	0.7331	0.3985	96.9
	$\beta_{21}$	0.1512	0.9988	0.8475	96.7	0.7102	1.7286	1.0184	96.4
	$\beta_{22}$	0.0884	1.0684	0.9800	96.9	0.7510	1.7219	0.9708	98.0
	α <sub>1</sub>	0.9413	2.0751	1.1338	96.4	0.8592	1.4087	0.5495	96.7
	$\alpha_2$	0.8820	2.1467	1.2648	95.9	0.8535	1.4337	0.5801	96.4
S.	$\beta_{11}$	0.1456	0.4164	0.2708	95.4	0.3137	0.6043	0.2906	97.5
53	$\beta_{12}$	0.1388	0.4250	0.2862	95.9	0.3051	0.5877	0.2826	97.1
	$\beta_{21}$	0.0779	1.1853	1.1074	95.1	0.7531	1.6888	0.9357	97.6
	$\beta_{22}$	0.0204	1.2588	1.2384	95.7	0.7500	1.7044	0.9544	98.0
	α <sub>1</sub>	0.9695	2.0515	1.0820	96.5	0.8551	1.4260	0.5709	96.0
	$\alpha_2$	0.9150	2.1136	1.1986	96.0	0.8687	1.3887	0.5199	97.2
S.	$\beta_{11}$	0.1446	0.4248	0.2803	95.6	0.3090	0.5935	0.2846	96.8
54	$\beta_{12}$	0.1381	0.4338	0.2957	95.1	0.3116	0.6016	0.2900	95.7
	$\beta_{21}$	0.0344	1.2142	1.1798	96.0	0.6549	1.6902	1.0354	96.1
	$\beta_{22}$	0.0000	1.2828	1.2828	96.6	0.7206	1.6900	0.9694	96.4
	α <sub>1</sub>	1.0953	1.8983	0.8029	95.2	0.7194	1.3198	0.6003	96.0
	$\alpha_2$	0.9670	2.1264	1.1595	96.8	0.7236	1.3356	0.6121	95.8
S-	$\beta_{11}$	0.1723	0.3951	0.2228	96.3	0.3615	0.7569	0.3953	97.7
5	$\beta_{12}$	0.1529	0.4019	0.2490	97.6	0.3313	0.7304	0.3991	95.8
	$\beta_{21}$	0.2317	0.9088	0.6771	97.0	0.7270	1.8336	1.1066	97.2
	$\beta_{22}$	0.1521	0.9730	0.8209	96.2	0.7162	1.6959	0.9798	95.9

**Table 15.** Interval estimates, AILs and CP(%) values of the ML and BE using MCMC for different schemes of progressive Type-II step-stress for NH distribution at n = 100 and m = 80

Sah	Dawm		Asy-	CI		HPD				
Scii.	r arm.	Lower	Upper	AIL	CP (%)	Lower	Upper	AIL	CP (%)	
	α <sub>1</sub>	1.0014	1.9767	0.9753	96.5	0.8672	1.4557	0.5885	96.1	
	$\alpha_2$	0.9671	2.0335	1.0663	96.5	0.8673	1.4477	0.5804	96.0	
<i>S</i> <sub>1</sub>	$\beta_{11}$	0.1370	0.4343	0.2973	95.5	0.2891	0.5819	0.2928	96.5	
	$\beta_{12}$	0.1385	0.4297	0.2912	95.6	0.3136	0.5886	0.2749	98.2	
	$\beta_{21}$	0.0000	1.2750	1.2750	95.6	0.6209	1.6470	1.0261	95.3	



Sch.	D	Asy-CI				HPD			
	Parm.	Lower	Upper	AIL	CP (%)	Lower	Upper	AIL	CP (%)
	$\beta_{22}$	0.0000	1.2940	1.2940	96.4	0.6088	1.6615	1.0528	96.3
c	$\alpha_1$	1.0260	1.9611	0.9351	97.8	0.8092	1.4226	0.6134	96.6
	$\alpha_2$	0.9928	2.0285	1.0357	96.9	0.7858	1.4112	0.6253	95.9
	$\beta_{11}$	0.1570	0.4077	0.2506	96.2	0.3278	0.6729	0.3450	98.2
52	$\beta_{12}$	0.1391	0.4231	0.2840	95.9	0.3121	0.6344	0.3223	96.9
	$\beta_{21}$	0.0896	1.0831	0.9935	95.3	0.6785	1.6941	1.0156	96.6
	$\beta_{22}$	0.0072	1.1713	1.1641	96.2	0.6988	1.7464	1.0475	96.9
	$\alpha_1$	0.9434	2.0292	1.0857	96.4	0.8707	1.4873	0.6166	96.3
S <sub>3</sub>	$\alpha_2$	0.9215	2.0581	1.1366	96.7	0.8537	1.4594	0.6058	95.9
	$\beta_{11}$	0.1437	0.4297	0.2860	95.5	0.3024	0.5890	0.2865	98.2
	$\beta_{12}$	0.1322	0.4443	0.3121	95.4	0.3068	0.5840	0.2773	97.3
	$\beta_{21}$	0.0000	1.3405	1.3405	96.1	0.5905	1.6456	1.0550	96.2
	$\beta_{22}$	0.0000	1.4175	1.4175	96.1	0.6994	1.7248	1.0254	98.2
	$\alpha_1$	0.9951	2.0382	1.0431	96.7	0.8963	1.4636	0.5673	96.9
	$\alpha_2$	0.9725	2.0632	1.0907	96.5	0.9054	1.4761	0.5707	97.2
S.	$\beta_{11}$	0.1580	0.3915	0.2335	95.8	0.2887	0.5656	0.2769	96.0
54	$\beta_{12}$	0.1407	0.4135	0.2728	95.5	0.3019	0.5778	0.2759	97.0
	$\beta_{21}$	0.0756	1.1268	1.0512	96.1	0.6619	1.6451	0.9832	96.0
	$\beta_{22}$	0.0000	1.2574	1.2574	96.8	0.7127	1.7442	1.0315	98.3
S <sub>5</sub>	$\alpha_1$	1.0603	1.9240	0.8637	97.2	0.7974	1.4596	0.6622	97.0
	$\alpha_2$	1.0173	2.0065	0.9891	96.3	0.8205	1.3699	0.5494	97.4
	$\beta_{11}$	0.1660	0.4001	0.2341	95.9	0.3001	0.6537	0.3536	96.4
	$\beta_{12}$	0.1493	0.4135	0.2642	95.9	0.3320	0.6646	0.3326	96.6
	$\beta_{21}$	0.1697	0.9853	0.8157	96.6	0.6779	1.6527	0.9748	96.3
	$\beta_{22}$	0.0591	1.1036	1.0445	97.0	0.7306	1.6954	0.9648	97.1

**Table 16.** Interval estimates, AILs and CP(%) values of the ML and BE using MCMC for complete sampling step-stress for NH distribution at n = 60,80 and 100

n	Dawm		Asy-	CI		HPD			
	rarm.	Lower	Upper	AIL	CP (%)	Lower	Upper	AIL	CP (%)
60	α <sub>1</sub>	1.0049	2.0198	1.0149	96.9	0.8616	1.4422	0.5805	96.0
	$\alpha_2$	0.9277	2.1227	1.1950	97.5	0.8508	1.4173	0.5664	96.1
	$\beta_{11}$	0.1411	0.4203	0.2792	95.1	0.3303	0.6326	0.3023	98.6
	$\beta_{12}$	0.1311	0.4305	0.2994	95.4	0.2952	0.6004	0.3051	96.1
	$\beta_{21}$	0.0383	1.1953	1.1570	95.1	0.6446	1.6218	0.9772	95.8
	$\beta_{22}$	0.0000	1.3433	1.3433	96.1	0.7458	1.7580	1.0122	98.1
	$\alpha_1$	1.0063	1.9930	0.9867	96.6	0.8337	1.4171	0.5834	95.2
	$\alpha_2$	0.9359	2.0793	1.1433	96.4	0.8462	1.4543	0.6081	95.8
Sa	$\beta_{11}$	0.1560	0.4069	0.2508	95.7	0.2855	0.5907	0.3052	96.3
52	$\beta_{12}$	0.1410	0.4253	0.2843	94.9	0.3037	0.5897	0.2861	96.8
	$\beta_{21}$	0.1043	1.0982	0.9939	95.1	0.6750	1.6353	0.9603	97.4
	$\beta_{22}$	0.0270	1.2010	1.1740	94.8	0.5959	1.6154	1.0195	95.8
<b>S</b> 3	α <sub>1</sub>	1.0603	1.9240	0.8637	97.2	0.7974	1.4596	0.6622	97.0
	$\alpha_2$	1.0173	2.0065	0.9891	96.3	0.8205	1.3699	0.5494	97.4
	$\beta_{11}$	0.1660	0.4001	0.2341	95.9	0.3001	0.6537	0.3536	96.4
	$\beta_{12}$	0.1493	0.4135	0.2642	95.9	0.3320	0.6646	0.3326	96.6
	$\beta_{21}$	0.1697	0.9853	0.8157	96.6	0.6779	1.6527	0.9748	96.3
	$\beta_{22}$	0.0591	1.1036	1.0445	97.0	0.7306	1.6954	0.9648	97.1



Parm.	MLE		BE MC	CMC: SEL	<b>BE MCMC: LINEX</b>		
	Est.	St.Er	Est.	St.Er	Est.: $v = -0.5$	Est.: $v = 0.5$	
$\beta_{11}$	1.7862	2.2538	0.8199	0.2420	0.8057	0.8350	
$\beta_{12}$	1.7121	2.8335	4.2366	2.9518	2.9924	7.2274	
$\beta_{21}$	1.1683	1.6557	3.1935	1.5610	2.7082	3.9038	
$\beta_{22}$	1.2362	2.3203	0.6495	0.3658	0.6175	0.6843	
α <sub>1</sub>	1.0885	1.9117	4.4086	1.9956	3.6670	5.6325	
α2	1.1502	2.6598	0.6431	0.4759	0.5895	0.7023	

Table 17. Est. and St.Ers of the ML and BE using MCMC for illustrative example

Table 18. Interval estimates and ILs values of the ML and BE using MCMC for an illustrative example

Dawm		Asy-CI		HPD			
r arm.	Lower	Upper	AIL	Lower	Upper	AIL	
$\beta_{11}$	0.0000	6.2035	6.2035	0.4279	1.2680	0.8402	
$\beta_{12}$	0.0000	7.2657	7.2657	1.1530	11.0140	9.8610	
$\beta_{21}$	0.0000	4.4133	4.4133	0.9345	6.2524	5.3178	
$\beta_{22}$	0.0000	5.7840	5.7840	0.1331	1.3129	1.1798	
$\alpha_1$	0.0000	4.8354	4.8354	1.4500	8.4061	6.9561	
$\alpha_2$	0.0000	6.3633	6.3633	0.0673	1.5143	1.4470	

# 8. Conclusion

In this paper, we studied a simple step-stress ALT model for the NH distribution under progressive Type-II censored data in the presence of competing causes of risks. We have derived the MLEs, and asymptotic confidence interval estimates for the unknown parameters. Also, we computed BEs and the corresponding HPD interval estimates under informative priors based on two different types of loss functions LINEX and squared error loss functions. We then conducted a simulation study to assess the performance of all these procedures and an explanatory instance has been offered to demonstrate all the methods of inference developed. The calculations have been made based on different sample sizes and five different progressive censoring schemes.

Finally, the simulation results demonstrate that both the MLEs and Bayesian estimates become better in terms of MSEs as the number of failures increases for fixed *n*. The MLEs and BEs for fixed sample size and pre-fixed number of failures increase, and the MSEs and Average estimate for unknown parameters decrease. The MLEs for scheme 5 have smaller MSEs than the other four schemes. Also, the MLEs for scheme 3 have the largest MSEs. The BEs of shape parameters  $\alpha_1$  and  $\alpha_2$  under LINEX loss function ( $\nu = 0.5$ ) have the smallest MSEs compared to estimates under the SE loss function, LINEX loss function ( $\nu = -0.5$ )). The BEs of scale parameters  $\beta_{11}$ ,  $\beta_{12}$ ,  $\beta_{21}$  and  $\beta_{22}$  under LINEX loss function ( $\nu = -0.5$ ) have the smallest MSEs as compared with estimates under the SE loss function and LINEX loss function ( $\nu = 0.5$ ) From the perspective of the confidence/credible intervals, the average lengths of all CIs and HPD credible intervals become smaller as m increases.

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